

General Disclaimer

One or more of the Following Statements may affect this Document

- This document has been reproduced from the best copy furnished by the organizational source. It is being released in the interest of making available as much information as possible.
- This document may contain data, which exceeds the sheet parameters. It was furnished in this condition by the organizational source and is the best copy available.
- This document may contain tone-on-tone or color graphs, charts and/or pictures, which have been reproduced in black and white.
- This document is paginated as submitted by the original source.
- Portions of this document are not fully legible due to the historical nature of some of the material. However, it is the best reproduction available from the original submission.

JSC-09434

NASA CR-

144355

PROGRAM DOCUMENTATION

SURFACE HEATING RATE OF THIN SKIN MODELS (THNSKN)

Program Q614

Job Order 83-157

(This revision supersedes 07000 dated November 1969)

(NASA-CR-144355) PROGRAM DOCUMENTATION: N75-28378
SURFACE HEATING RATE OF THIN SKIN MODELS
(THNSKN) (Lockheed Electronics Co.) 81 p HC
\$4.75 CSCL 20M Unclas
G3/34 31068

Prepared By

Lockheed Electronics Company, Inc.

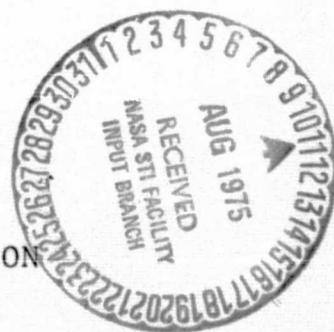
Aerospace Systems Division

Houston, Texas

Contract NAS 9-12200

For

INSTITUTIONAL DATA SYSTEMS DIVISION



National Aeronautics and Space Administration
LYNDON B. JOHNSON SPACE CENTER
Houston, Texas

April 1975

LEC-5523

PROGRAM DOCUMENTATION
SURFACE HEATING RATE OF THIN SKIN MODELS (THNSKN)

Program Q614

Job Order 83-157

PREPARED BY

Jack D. McBryde
Jack D. McBryde
Lockheed Electronics Company, Inc.

APPROVED BY

LEC

NASA

C E Hutchinson
C. E. Hutchinson, Supervisor
On-Site Processing Section

Walter D. Poates
W. D. Poates, Technical
Monitor, Data Processing
Branch

W N Fitzpatrick
W. N. Fitzpatrick, Acting
Manager, Data Processing
Systems Department

Prepared By
Lockheed Electronics Company, Inc.

For

Institutional Data Systems Division

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
LYNDON B. JOHNSON SPACE CENTER
HOUSTON, TEXAS

April 1975

LEC-5523

TECHNICAL REPORT INDEX/ABSTRACT
(See instructions on reverse side.)

1. TITLE AND SUBTITLE OF DOCUMENT

Program Documentation
 Surface Heating Rate of Thin Skin Models (THNSKN)

2. JSC NO.

JSC-09434

3. CONTRACTOR/ORGANIZATION NAME

Lockheed Electronics Company, Inc.

4. CONTRACT OR GRANT NO.

NAS 9-12200

5. CONTRACTOR/ORIGINATOR DOCUMENT NO.

LEC-5523

6. PUBLICATION DATE (THIS ISSUE)

April 1975

7. SECURITY CLASSIFICATION

Unclassified

8. OPR (OFFICE OF PRIMARY RESPONSIBILITY)

J. E. Wakeland

9. LIMITATIONS

GOVERNMENT HAS UNLIMITED RIGHTS YES NO

IF NO, STATE LIMITATIONS AND AUTHORITY

10. AUTHOR(S)

Jack D. McBryde

11. DOCUMENT CONTRACT REFERENCES

12. HARDWARE CONFIGURATION

WORK BREAKDOWN STRUCTURE NO.

SYSTEM

N/A

N/A

CONTRACT EXHIBIT NO.

SUBSYSTEM

N/A

N/A

DRL NO. AND REVISION

MAJOR EQUIPMENT GROUP

N/A

N/A

DRL LINE ITEM NO.

N/A

13. ABSTRACT

THNSKN computes the mean heating rate at a maximum of 100 locations on the surface of thin skin transient heating rate models. Output is printed in tabular form and consists of time history tabulation of temperatures, average temperatures, heat loss without conduction correction, mean heating rate, least squares heating rate, and the percent standard error of the least squares heating rates. The input tape used is produced by the program EHTS03.

14. SUBJECT TERMS

ARC JET

THERMOCOUPLES

HEATING RATE

THIN SKIN

TABLE OF CONTENTS

	Page
UNIT I PROGRAM ABSTRACT AND HISTORY OF USE.	1
A. Abstract	1
B. Program History.	1
UNIT II PROGRAM USERS INFORMATION.	2
A. Identification	2
B. Description of Program Request	2
C. Usage.	2
D. Analysis	4
E. Flow Chart	11
F. Storage Requirements	11
G. List of Subroutines.	11
H. Location of Source and Binary Decks.	11
I. Program Listing.	11
J. Correspondence	11

LIST OF ATTACHMENTS

<u>Number</u>	<u>Titles</u>
1	Lead Card Setup
2	Deck Setup
3	Run Request Card
4	Flow Chart
5	Program Listing
6	Sample Input
7	Sample Output
8	Correspondence
9	Diagnostic Messages

UNIT I
PROGRAM ABSTRACT AND HISTORY OF USE

A. ABSTRACT

Program THNSKN computes the mean heating rate at a number of thermocouple locations on the surface of thin skin transient heating rate models. Experimental data, calibrated in engineering units, is obtained from ABEL tape output of the EHTS03 data reduction computer program. The program output consists of time history tabulations in an array by thermocouple locations for each time sample.

B. PROGRAM HISTORY

The original THNSKN program was written in 1969. The current version was written in December 1974 as requested by SCR83-15-30.

UNIT II
PROGRAM USERS INFORMATION

A. IDENTIFICATION

Title: Surface Heating Rate of Thin Skin Models (THNSKN)
Author: Jack D. McBryde
Date: December 1974
Installation: JSC, Houston, Texas
Authorization: Contract NAS 9-12200
Source Language: FORTRAN V
Computer Configuration: UNIVAC 1108 or 1110, EXEC 8

B. DESCRIPTION OF PROGRAM REQUEST

See attachment 8.

C. USAGE

1. Input Requirements and Data Descriptions:

The THNSKN input tape is produced by the program EHTS03. It is a FORTRAN-written binary tape containing time in floating-point seconds followed by data in floating point for N channels. The number of channels (N) is fixed for a given tape ($N \leq 259$).

See attachment 6 for sample input.

2. Lead Card Setup:

See attachment 1.

3. Deck Setup:

See attachment 2.

4. Tape Assignments:

See attachment 3.

5. Restrictions:

The following list is a summary of the restrictions:

- The input tape must have the format specified in section C.1.
- The array of thermocouples must have no more than 50 rows or columns, and one row or column must contain at least three thermocouples.
- Each specified time slice must contain at least three input records.
- The maximum number of points for thermocouples, which may be used for least squares heat loss computations, is 50.

6. Diagnostic, Normal-Console, and Standard-Output Messages:

See attachment 9.

7. Labels, Save-Tapes, and Output Disposition:

There is printer output only.

8. Output Formats:

See attachment 7.

9. Nonstandard System Requirements:

There are none.

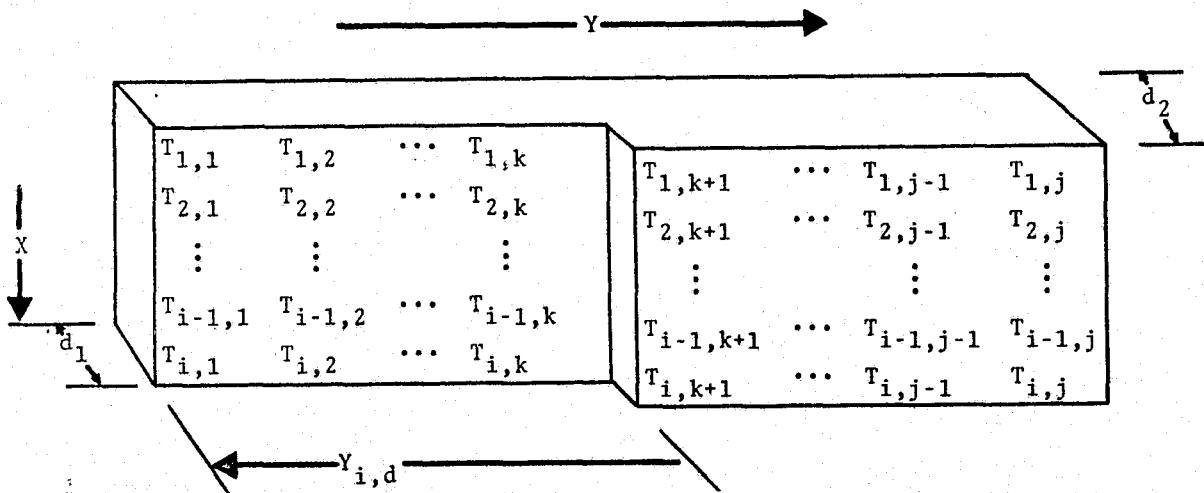
10. Running Time:

THNSKN processes nine thermocouples for 40 time points in less than 1/2 minute.

D. ANALYSIS

1. Description of the Relationship of Variables to the Test Item:

The test item may be considered to be a rectangular plate having, at most, two thicknesses as shown:



- The origin of the x -, y -coordinate system is the upper left corner.

- The variables d_1 and d_2 are the two thicknesses. If the test item has only one thickness, it is represented by d .
- The variable $T_{i,j}$ is the temperature at a thermocouple in degrees Fahrenheit.
- The variables $T_{i,k}$ and $T_{i,k+1}$ are temperatures adjacent to the thickness difference junction.
- The variable $Y_{i,d}$ is the y-coordinate of the junction at row i in inches.
- Each row or column is colinear in the X-, Y-plane so that the coordinates of all the thermocouples (X , Y) can be expressed using i-values of X and j-values of Y . Both X and Y are in inches.

2. Equations:

2.1 Mean temperatures:

The mean temperature \bar{T} for each thermocouple is computed by

$$\bar{T} = \frac{1}{N} \sum_{\ell=1}^N T_{\ell} \quad (1)$$

where N is the number of temperatures read in the time interval processed.

2.2 Mean heat flux without conduction correction:

The mean heat flux without conduction correction \bar{q} is computed by

$$\bar{q}_{i,j} = \frac{\rho C_p d}{24(t_N - t_1)} \frac{N-1}{N-2} \left(T_{i,j}^N + T_{i,j}^{N-1} - T_{i,j}^1 - T_{i,j}^2 \right) \quad (2)$$

where

t_1 = the time for the first scan of data in the interval in seconds.

t_N = the time for the last scan of data in the interval in seconds.

$T_{i,j}^1, T_{i,j}^2, T_{i,j}^{N-1}, T_{i,j}^N$ = the first, second, next to the last, and last temperatures of the thermocouple in row i and column j.

ρ = mass density in lb/ft^3 .

C_p = specific heat in $BTU/lb^{\circ}F$.

d = thickness of test material in inches.

If the test item has two thicknesses, then $d = d_1$ for $j \leq k$ (see the figure) and $d = d_2$ for $j > k$.

2.3 Mean lateral heat loss in the X-direction:

The mean lateral heat loss in the X-direction \bar{q}^x is computed by

$$\bar{q}_{i,j}^x = \frac{24Kd}{X_{i+1} - X_{i-1}} \left(\frac{\bar{T}_{i,j} - \bar{T}_{i-1,j}}{X_i - X_{i-1}} - \frac{\bar{T}_{i+1,j} - \bar{T}_{i,j}}{X_{i+1} - X_i} \right) \quad (3)$$

where

K = thermal conductivity in BTU/ft sec°F.

$d = d_1$ for $j \leq k$ (see the figure).

$d = d_2$ for $j > k$.

2.4 Mean lateral heat loss in the Y-direction:

The mean lateral heat loss in the Y-direction \bar{q}^y may be computed by one of three equations, depending on whether the test material has one or two thicknesses and the position of the thermocouple relative to the junction between the thicknesses.

Case 1: The variable \bar{q}^y when the material has one thickness or where it has two and all three thermocouples are the same side of the junction.

$$\bar{q}_{i,j}^y = \frac{24Kd}{Y_{j+1} - Y_{j-1}} \left(\frac{\bar{T}_{i,j} - \bar{T}_{i,j-1}}{Y_j - Y_{j-1}} - \frac{\bar{T}_{i,j+1} - \bar{T}_{i,j}}{Y_{j+1} - Y_j} \right) \quad (4)$$

where

$$d = d_1 \text{ when } j + 1 \leq k .$$

$$d = d_2 \text{ when } j - 1 > k .$$

Case 2: The variable \bar{q}^y when the material has two thicknesses and $j = k$ (see the figure).

$$\bar{q}_{i,j}^y = \frac{24Kd_1}{Y_{k+1} - Y_{k-1}}$$

$$\left(\frac{\bar{T}_{i,k} - \bar{T}_{i,k-1}}{Y_k - Y_{k-1}} - \frac{d_2(\bar{T}_{i,k+1} - \bar{T}_{i,k})}{(Y_d - Y_k)d_2 + (Y_{k+1} - Y_d)d_1} \right)$$

(5)

where

Y_d = the Y-coordinate of the function at row i (see the figure).

Case 3: The variable \bar{q}^y when the material has two thicknesses and $j = k + 1$.

$$\bar{q}_{i,j}^y = \frac{24Kd_2}{Y_{k+2} - Y_k}$$

$$\left(\frac{d_1(\bar{T}_{i,k+1} - \bar{T}_{i,k})}{(Y_d - Y_k)d_2 + (Y_{k+1} - Y_d)d_1} - \frac{\bar{T}_{i,k+2} - \bar{T}_{i,k+1}}{Y_{k+2} - Y_{k+1}} \right)$$

(6)

2.5 Mean heating rate:

The mean heating rate $\bar{\dot{q}}$ is computed from equations 2, 3, and 4, 5, or 6.

$$\bar{\dot{q}}_{i,j} = \bar{\dot{q}}_{i,j} + \bar{q}_{i,j}^x + \bar{q}_{i,j}^y \quad (7)$$

3. Special Treatment When the Array Contains Bad Thermocouples:

The variables $\bar{\dot{q}}$, \bar{q} , \bar{q}^x and \bar{q}^y are not computed for bad thermocouples. These values are set to zero.

In computing \bar{q}^x for a column containing one or more bad thermocouples, temperatures and x-coordinates of three successive good (but not necessarily adjacent) thermocouples are used.

The same procedure is used in computing \bar{q}^y .

4. The Variables \bar{q}^x and \bar{q}^y at Row or Column End Points:

The conduction correction (\bar{q}^x or \bar{q}^y) used at the end points (first or last good thermocouple) are the same as those computed for the adjacent thermocouple in the row or column.

5. Linear Least Squares Heating Rate and Percent Standard Error:

The heating rate at each thermocouple \bar{Q} is computed from the slope M by

$$\bar{\dot{Q}} = \frac{\rho C_p d}{12} M \quad (8)$$

The slope M is computed by

$$M = \frac{n \sum t_i T_i - \sum t_i \sum T_i}{n \sum t_i^2 - (\sum t_i)^2} \quad (9)$$

where

n = the number of scans.

t = time.

T = temperature.

The percent standard error E is computed by

$$E = \frac{S_n(M)}{M} \times 100 \quad (10)$$

$$S_n(M) = n \sigma_n(T) \left\{ (n - 2) \left[n \sum t_i^2 - (\sum t_i)^2 \right] \right\}^{1/2} \quad (11)$$

$$\sigma_n(T) = \frac{1}{n}$$

$$\left\{ n \sum T_i^2 - (\sum T_i)^2 - \frac{(n \sum t_i T_i - \sum t_i \sum T_i)^2}{n \sum t_i^2 - (\sum t_i)^2} \right\}^{1/2} \quad (12)$$

If the time slice specified contains more than n scans, the last time and corresponding temperatures are used as the first time and temperatures for the next n scans.

E. FLOW CHART

See attachment 4.

F. STORAGE REQUIREMENTS

Forty-three thousand decimal locations are required.

G. LIST OF SUBROUTINES

None.

H. LOCATION OF SOURCE AND BINARY DECKS

The Data Processing Systems Department of Lockheed Electronics Company, Inc., maintains all source and binary decks for this program.

I. PROGRAM LISTING

See attachment 5.

J. CORRESPONDENCE

See attachment 8.

ATTACHMENT 1

LEAD CARD SETUP

PRECEDING PAGE BLANK NOT FILMED

LEAD CARD SETUP

CARD NO. 1

JOB _____

NAME THNSKN

PROGRAMMER McBryde **DATE** 12/74

PAGE 1 OF 10

DATE 12/74

LEAD CARD SETUP

CARD NO. 2

JOB _____

NAME THNSKN

PROGRAMMER McBryde **DATE** 12/74

PAGE 2 OF 10

DATE 12/74

CONSTANTS

LEAD CARD SETUP

CARD NO. 3

JOB _____

PAGE 3 OF 10

NAME THNSKN

PROGRAMMER McBryde **DATE** 12/74

Comment: *A minimum of a 1×3 or 3×1 array of x, y-coordinates is required.

MISCELLANEOUS RUN PARAMETERS

LEAD CARD SETUP

CARD NO. 4

JOB _____

NAME THNSKN

PROGRAMMER McBryde

PAGE 4 OF 10

DATE 12/74

Comment: *The input tape record has a time word preceding the data channels. These numbers do not include the time word.

Y-COORDINATES OF THICKNESS DIFFERENCE JUNCTION

LEAD CARD SETUP

CARD NO. 5

JOB _____

NAME THNSKN

PROGRAMMER McBryde **DATE** 12/74

PAGE 5 OF 10

DATE 12/74

Comment: Use as many cards as required to define NX values.

X - COORDINATES

LEAD CARD SETUP

CARD NO. 6

JOB _____

PAGE 6 OF 10

NAME THNSKN

PROGRAMMER McBryde DATE 12/74

Comment: Enter as many cards as needed to define NX locations
($NX \leq 50$).

Y - COORDINATES

LEAD CARD SETUP

CARD NO. 7

JOB _____

PAGE 7 OF 10

NAME THNSKN

PROGRAMMER McBryde DATE 12/74

Comment: Enter as many cards as required to define NY locations
(NY \leq 50).

THERMOCOUPLE CHANNEL NUMBERS

LEAD CARD SETUP

CARD NO. 8

JOB _____

NAME THNSKN

PROGRAMMER McBryde

PAGE 8 OF 10
DATE 12/74

Comment: Enter as many cards as needed to define NX * NY thermo-couple locations. Bad thermocouples should be indicated with NTCH (IX,IY) = 0 .

START - STOP TIMES

LEAD CARD SETUP

CARD NO. 9

JOB _____

PAGE 9 OF 10

NAME THNSKN

PROGRAMMER McBryde DATE 12/74

COMMAND EVENT START - STOP

LEAD CARD SETUP

CARD NO. 9A

JOB _____

NAME THNSKN

PROGRAMMER McBryde DATE 12/74

PAGE 10 OF 10

ATTACHMENT 2

DECK SETUP

DECK SETUP FOR PROGRAM THNSKN (EXEC VIII)

PAGE NO. 1 OF 1

(Back of deck)

7
8 PMD, E

One or more card 9A's if IOPT1
on card 4 is 1.

One or more card 9's if IOPT1
on card 4 is 0.

CARDS 6 - 8

CARD 5 [Only if DD(2) on card 3 > 0]

THNSKN CARDS 1 - 4

7
8XQT .THNSKN/ABS

7
8MAP,S .THNSKN,THNSKN/ABS

7
8PREP

7
8COPIN PGMTP,TPF\$

7
8ASG,T 8,8C,XXXXXX (Input tape number)

7
8ASG,T PGMTP,8C,V02679

7
8MSG,N TWO TAPE DRIVES

7
8RUN

(Front of deck)

ATTACHMENT 3

RUN REQUEST FORM

INSTRUCTIONS FOR CENTRAL COMPUTER COMPLEX COMPUTER RUNS

RUNID

PROGRAMMER'S COMMENTS:

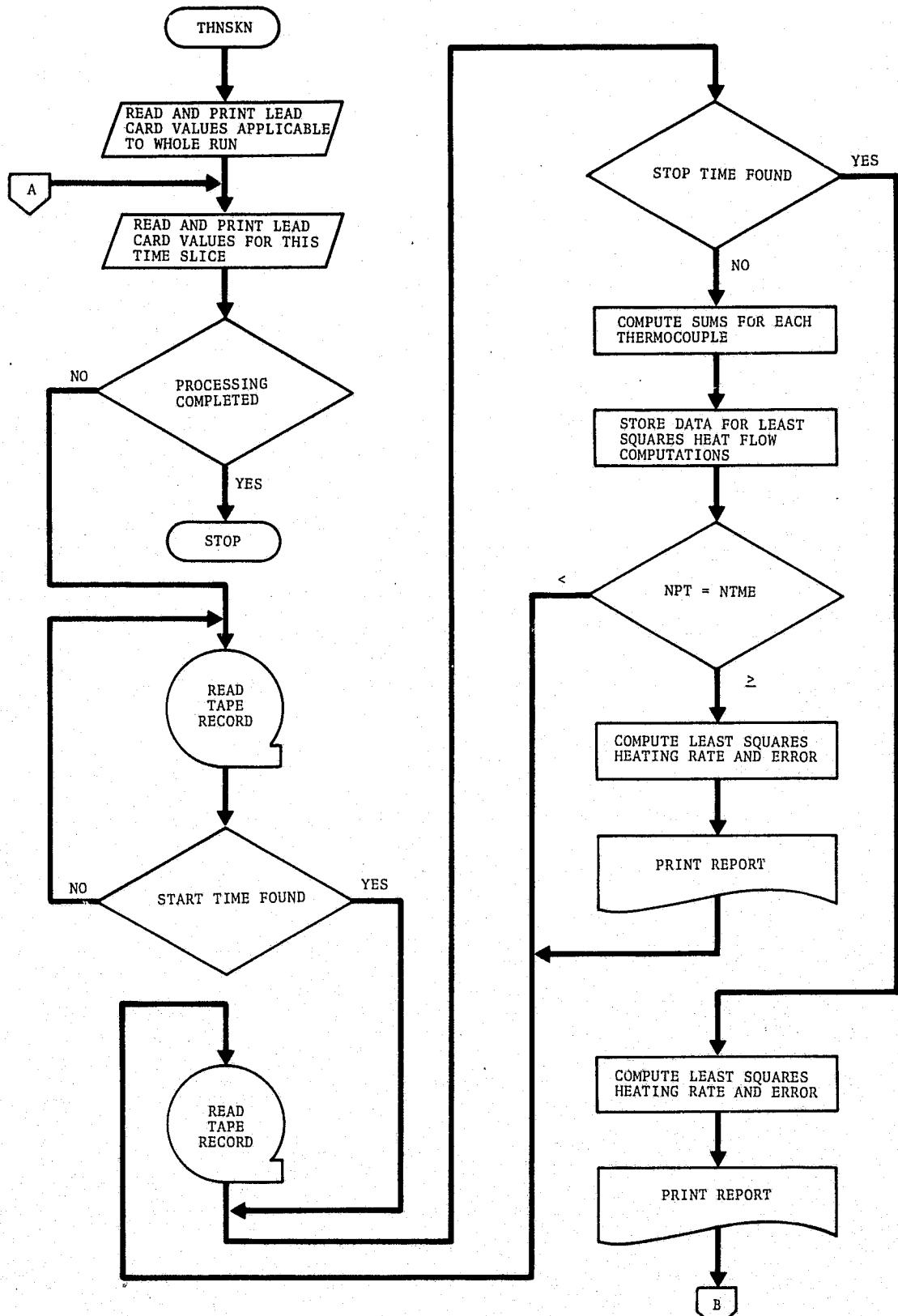
(DO NOT FILL IN SHADDED AREAS)

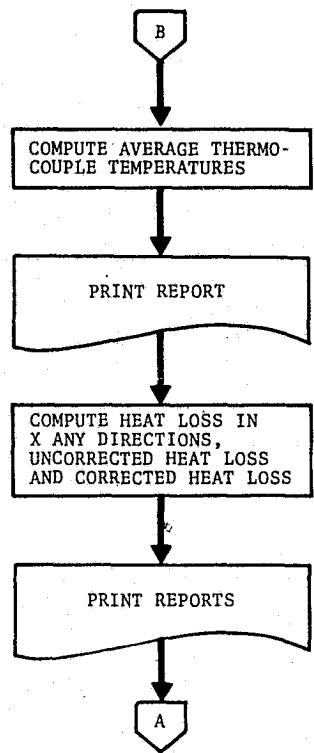
EXEC VIII

PROGRAMMER XXXXXX			BADGE NO. XXXX	BOX NO. XXX	PHONE NO. XXX	DATE XXX	PRIORITY & INITIALS <i>[Shaded area]</i>		
DIVISION CODE FDXX	PHOG. NO Q614	PROJ. NO. XXXX	EST. TIME XX	MAX. TIME XX	PAGES OUTPUT XX	SEG. NO.			
OPERATING SYSTEM			TYPE OF RUN			NO. TAPES 2	NO. FASTR FILES 0	NO. DRUM FILES 0	
1108 EXEC II <input type="checkbox"/> 3200 SCOPE <input type="checkbox"/>			PROD <input checked="" type="checkbox"/> TEST <input type="checkbox"/>						
1108 EXEC VIII <input checked="" type="checkbox"/> 3200 SMARTS <input type="checkbox"/>			OTHER EXPLAIN BELOW						
1108 COBOL <input type="checkbox"/> 3200 OTHER <input type="checkbox"/>									
INPUT TAPES			WORKING TAPES	OUTPUT TAPES			PERMANENT FASTRAND FILES		
UNIT	REEL NO.	FILE NAME		UNIT	REEL NO.	FILE NAME	SAVE	\$	\$
A PROGRAM TAPE							\$	\$	
							\$	\$	
F XXXXXX							\$	\$	
							\$	\$	
							\$	\$	
4060 <input type="checkbox"/>			REEL NO.	FILE NO.	PUNCHED OUTPUT <input type="checkbox"/>	PEEL NO.	NO. CARDS		
18 MM <input type="checkbox"/> 35 MM <input type="checkbox"/>									
CAL COMP PLOT <input type="checkbox"/>			PRINT TYPE	NU. PLOTS	ACTUAL TIME USAGE				
ANOMALY REPORT			SYSTEM NO. <input type="checkbox"/>		STOP <input type="checkbox"/>				
EXEC OUTPUT <input type="checkbox"/>			SYSTEM NO. <input type="checkbox"/>		START <input type="checkbox"/>				
EXC. LST TIME <input type="checkbox"/>			PUNCH OUTPUT <input type="checkbox"/>						
GET ORG. EXEC. APP. TO EXEC. <input type="checkbox"/>									
DETAILED EXECUTIONS									

ATTACHMENT 4

FLOW CHART





ATTACHMENT 5

PROGRAM LISTING

GFOR:15 THNSKN, THNSKN
FOR SEIX-12/20/74-03:02:19 (,0)

MAIN PROGRAM

STORAGE USED: CODE(1) 003717; DATA(0) 073316; BLANK COMMON(2) 0000000

EXTERNAL REFERENCES (BLOCK, NAME)

0003	EXIT
0004	CHERR
0005	NINTRS
0006	NRDUS
0007	NI03S
0010	NI02S
0011	NRDUS
0012	NI01S
0013	NERR2S
0014	NRBUS
0015	NSTOPS
0016	DSQRT
0017	NERR4S
0020	NERR3S

ORIGINAL PAGE 16
OF FOUR QUALITY

STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

0001	000150	10L	0000	072335	1000F	0000	072336	1001F	0000	072340	1002F	0000	072341	1003F
0000	072343	1004F	0000	072346	1005F	0000	072350	1007F	0000	072352	1008F	0001	001727	1014F
0001	001741	1022G	0001	001750	1027G	0001	001774	1041G	0001	002006	1047G	0001	002015	1054G
0001	000677	110L	0001	002105	1103G	0001	002117	1111G	0001	002122	1114G	0001	002141	1126G
0001	002154	1134G	0001	002155	1137G	0001	002175	1153G	0001	000705	120L	0001	002375	1236G
0001	032407	1244G	0001	002416	1251G	0001	002446	1264G	0001	000724	130L	0001	003005	1371G
0001	003017	1377G	0001	000732	140L	0001	003026	1404G	0001	003072	1415G	0001	003076	1421G
0001	003157	1453G	0001	003171	1461G	0001	003200	1466G	0001	000743	150L	0001	003224	1500G
0001	003236	1506G	0001	003245	1513G	0001	003331	1537G	0001	003352	1550G	0001	003354	1553G
0001	003366	1562G	0001	000752	160L	0001	003446	1647G	0001	003504	1660G	0001	003513	1663G
0001	003545	1677G	0001	000757	170L	0001	003630	175L	0001	001003	190L	0001	000227	20L
0001	003632	200L	0000	072354	2000F	0000	072360	2001F	0000	072455	2002F	0000	072527	2003F
0000	072564	2004F	0000	072624	2005F	0000	072634	2006F	0000	072644	2007F	0000	072654	2008F
0000	072663	2009F	0000	072675	2010F	0000	072704	2011F	0000	072716	2012F	0000	072724	2013F
0000	072736	2014F	0000	072751	2015F	0000	072770	2016F	0000	072777	2017F	0000	073010	2018F
0000	073034	2019F	0000	073051	2020F	0000	073066	2021F	0000	073047	2022F	0000	073107	2023F
0001	001056	220L	0001	000243	221G	0001	000255	227G	0001	001075	230L	0001	000304	236G
0001	001112	240L	0001	000316	244G	0001	001121	250L	0001	000330	252G	0001	000342	260G
0001	001126	260L	0001	000353	266G	0001	001152	280L	0001	000261	30L	0001	000401	300G
0001	001170	300L	0001	000413	306G	0001	000422	313G	0001	001242	330L	0001	001267	340L
0001	001363	365L	0001	001424	370L	0001	001572	395L	0001	001614	400L	0000	073127	4001F
0000	073135	4002F	0000	073145	4003F	0000	073154	4004F	0000	073165	4005F	0001	000410	405G
0001	000611	407G	0001	001653	410L	0001	000654	426G	0001	002026	440L	0001	000717	444G
0001	001010	476G	0001	002207	480L	0001	002227	490L	0001	000445	50L	0001	002247	500L
0001	002355	510L	0001	001052	512G	0001	001070	523G	0001	002427	530L	0001	002453	540L
0001	002473	550L	0001	001165	560G	0001	002513	560L	0001	001175	566G	0001	002544	570L
0001	002557	575L	0001	002614	580L	0001	002656	590L	0001	000502	60L	0001	001235	600G
0001	002717	600L	0001	002761	610L	0001	001315	627G	0001	003037	630L	0001	001332	636G
0001	003131	640L	0001	001335	641G	0001	003137	650L	0001	001352	651G	0001	003256	680L

0001	003270	690L	0001	000536	70L	0001	001473	705G	0001	001505	713G	0001	001514	720G
0001	003404	730L	0001	001540	732G	0001	001552	740G	0001	001561	745G	0001	001606	756G
0001	000555	80L	0001	003642	999L	0000	073210	9999F	0000 R	072255	B1GK	0000 R	072301	CESTOP
0000 R	072300	CESTRT	0000 R	072303	C0N12	0000 R	072304	C0N24	0000 R	072302	C0N6	0000 R	072254	CP
0000 R	072130	0D	0000 R	065224	ERR	0000 R	072333	FAC	0000 I	072266	I	0000 I	072245	IBL
0000 I	072317	1DD	0000 I	072250	EOF	0000 I	072311	IESTOP	0000 I	072310	IESTRT	0000 I	072315	IEVNT
0000 I	072320	1GO00P	0000	073247	INJPS	0000 I	072273	I0PT	0000 I	072263	I0PT1	0000 I	072305	IPAR
0000 I	072270	1X	0000 I	072271	IY	0000 I	072314	IYD0	0000 I	072321	II	0000 I	072323	I2
0000 I	072325	I3	0000 I	072267	J	0000 I	072247	JEQ	0000 I	072327	J1	0000 I	072330	J2
0000 I	072331	J3	0000 I	072252	LCDERR	0000 I	072313	LINES	0000 I	072307	LTEMP	0000 I	072251	LUIN
0000 I	072334	M	0000 I	072272	N	0000 I	072262	NCC	0000 I	072261	NCHS	0000 I	072316	NN
0000 I	072322	NN1	0000 I	072324	NN2	0000 I	072326	NN3	0000 I	072265	NOTH	0000 I	072267	NPAR
0000 I	072312	NPT	0000 I	072306	NSCN	0000 I	000174	NTCH	0000 I	072260	NTCLOC	0000 I	072277	NTME
0000 I	072296	NTSL	0000 I	072256	NX	0000 I	072257	NY	0000 R	022022	QDOT	0000 R	026726	QDOTMM
0000 R	010212	0X	0000 R	015116	QY	0000 R	072253	RHO	0000 D	072243	SERR	0000 D	072241	SIGMA
0000 D	072237	SLOPE	0000 R	072276	STATME	0000 D	072217	SUM1	0000 D	072221	SUM2	0000 D	072233	SUM3
0000 D	072225	SUM4	0000 D	072227	SUM5	0000 D	072231	SUM6	0000 D	072233	SUM7	0000 D	072235	SUM8
0000 R	005100	TEMP	0000 R	033632	TIM	0000 R	072132	TIME	0000 R	000000	TITLE1	0000 R	0000014	TITLE2
0000 R	033714	TMP	0000 R	072275	TSTOP	0000 R	072274	TSTRT	0000 R	010130	WORD	0000 R	000030	WX
0000 R	072133	YDD	0000 R	000112	YY	0000 R	072132	YVD						

00100	10	C	PROGRAM THNSKN
00100	20	C	
00100	30	C	IDENTIFICATION
00100	40	C	TITLE - SURFACE HEATING RATE OF THIN SKIN MODELS
00100	50	C	PROGRAMMER - JACK D. MCBRYDE, LOCKHEED ELECTRONICS CO.
00100	60	C	DATE - OCTOBER 1969, REWRITTEN DECEMBER 1974
00100	70	C	INSTALLATION - NASA JSC HOUSTON TEXAS
00100	80	C	
00100	90	C	DESCRIPTION
00100	100	C	THE PROGRAM COMPUTES THE HEATING RATE AT A NUMBER OF LOCATIONS
00100	110	C	ON THE SURFACE OF THIN SKIN TRANSIENT HEATING RATE MODELS.

EXPERIMENTAL DATA, CALIBRATED IN ENGINEERING UNITS, IS OBTAINED FROM THE ABEL TAPE OUTPUT OF THE EHTS03 DATA REDUCTION COMPUTER PROGRAM. THE PROGRAM OUTPUT CONSISTS OF TIME HISTORY TABULATION IN AN ARRAY BY THERMOCOUPLE LOCATIONS.

GK - THERMAL CONDUCTIVITY (K) OF TEST MATERIAL (BTU/FT.SEC F)

STOP - COMMAND EVENT CHANNEL STOP LEVEL INPUT (FLOATING POINT)
STRT - COMMAND EVENT CHANNEL START LEVEL INPUT (FLOATING POINT)

N12 - RHO + CP / 12.

N24 - 2400 BIGK

- SPECIFIC HEAT OF TEST MATERIAL (BTU/FT² SEC.)

(1) - SKIN THICKNESS OF TEST MATERIAL (INCHES)

(2) - THE SECOND THICKNESS WHEN THE TEST MATERIAL HAS TWO

- PERCENT ERROR IN THE SLOPE
- USED TO DESIGNATE COORDINATE IN X-DIRECTION

D - INDEX USED TO SPECIFY WHICH THICKNESS (DD) APPLIES

OF THE END OF FILE INDICATOR

~~STOP - COMMAND EVENT CHANNEL STOP LEVEL (FIXED POINT)~~

THE COUNCIL OF THE AMERICAN LIBRARY ASSOCIATION

[View Details](#) | [Edit](#) | [Delete](#)

Digitized by srujanika@gmail.com

ORIGINAL PAGE IS
OF POOR QUALITY

ORIGINAL PAGE IS
OF POOR QUALITY

00100	34*	C	IEVNT	- CURRENT COMMAND EVENT CHANNEL VALUE	000000
00100	35*	C	IGOOD	- IGOOD = 1 INDICATES WHEN THE FIRST SET OF 3 GOOD THERMO-	000000
00100	36*	C		COUPLES IN A ROW OR COLUMN HAS BEEN FOUND IN LOGIC FOR	000000
00100	37*	C		COMPUTING QX OR QY	000000
00100	38*	C	IOPT	- RUN CONTROLLED BY 0 - START-STOP TIMES	000000
00100	39*	C		1 - COMMAND CHANNEL EVENTS	000000
00100	40*	C	IOPTI1	- IOPT + 1	000000
00100	41*	C	IPAR	- PARITY ERROR RECORD COUNTER	000000
00100	42*	C	IX	- X-COORDINATE OF THERMOCOUPLE BEING DEFINED BY CHANNEL NO.	000000
00100	43*	C	IY	- Y-COORDINATE OF THERMOCOUPLE BEING DEFINED BY CHANNEL NO.	000000
00100	44*	C	IYDD	- THE Y COORDINATE INDEX JUST PRIOR TO THE CHANGE IN	000000
00100	45*	C		MATERIAL THICKNESS	000000
00100	46*	C	I1,I2,I3	- THE INDICES FOR 3 SUCCESSIVE (BUT NOT NECESSARILY	000000
00100	47*	C		ADJACENT) LOCATIONS OF GOOD THERMOCOUPLES IN THE X	000000
00100	48*	C		DIRECTION	000000
00100	49*	C	J	- USED TO DESIGNATE COORDINATES IN Y-DIRECTION	000000
00100	50*	C	J1,J2,J3	- SAME AS I1,I2,I3 BUT IN Y DIRECTION	000000
00100	51*	C	LCDERR	- LEAD CARD ERROR INDICATOR	000000
00100	52*	C	LINES	- LINE COUNTER FOR PAGE EJECT CONTROL	000000
00100	53*	C	LTEMP	- NUMBER OF LINES REQUIRED FOR ONE NX X NY ARRAY	000000
00100	54*	C	LUIN	- LOGICAL UNIT FOR INPUT TAPE	0C0000
00100	55*	C	NC	- THE MAXIMUM NUMBER OF CHANNELS THE INPUT TAPE MAY HAVE	000000
00100	56*	C	NCC	- NUMBER OF COMMAND CHANNEL	000000
00100	57*	C	NCHS	- NUMBER OF CHANNELS ON TAPE	000000
00100	58*	C	NLS	- THE MAXIMUM NUMBER OF SCANS FOR WHICH LEAST SQUARES	000000
00100	59*	C		COMPUTATIONS MAY BE DONE	000000
00100	60*	C	NN	- CHANNEL NUMBER OF THERMOCOUPLE BEING PROCESSED	000000
00100	61*	C	NN1,NN2,NN3	- CHANNEL NUMBERS OF THREE SUCCESSIVE GOOD THERMO-	000000
00100	62*	C		COUPLES (QX OR QY COMPUTATIONS)	000000
00100	63*	C	NOTH	- TIME HISTORY TAB OPTION. IF NOTH = 0, EACH SCAN OF DATA	000000
00100	64*	C		FROM THE INPUT TAPE IN THE TIME INTERVAL WILL BE PRINTED.	000000
00100	65*	C	NPAR	- MAXIMUM PERMISSIBLE NUMBER OF PARITY ERRORS PER TIME	000000
00100	66*	C		SLICE	000000
00100	67*	C	NPT	- NUMBER OF POINTS USED IN THE CURVE FIT	000000
00100	68*	C	NSCN	- NUMBER OF SCANS OF DATA PROCESSED IN THE CURRENT TIME	000000
00100	69*	C		SLICE	000000
00100	70*	C	NTCH	- ARRAY OF THERMOCOUPLE CHANNEL NUMBERS	000000
00100	71*	C	NTCLOC	- TOTAL NUMBER OF THERMOCOUPLE LOCATIONS (NX * NY)	000000
00100	72*	C	NTME	- NUMBER OF POINTS REQUESTED FOR CURVE FIT	000000
00100	73*	C	NTSL	- NUMBER OF TIME SLICES PROCESSED	000000
00100	74*	C	NX	- NUMBER OF X-COORDINATE LOCATIONS	000000
00100	75*	C	NY	- NUMBER OF Y-COORDINATE LOCATIONS	000000
00100	76*	C	QDOT	- USED FOR MEAN HEATING RATE AND LEAST SQUARES HEATING RATE AT	000000
00100	77*	C		DIFFERENT TIMES	000000
00100	78*	C	QDOTMM	- THE SUMS (OR AVERAGES) OF THE QDOT VALUES FOR NTSL TIME	000000
00100	79*	C		SLICES	000000
00100	80*	C	QX	- MEAN LATERAL HEAT LOSS IN X DIRECTION	000000
00100	81*	C	QY	- MEAN LATERAL HEAT LOSS IN Y DIRECTION	000000
00100	82*	C	RHO	- MASS DENSITY OF TEST MATERIAL (LBH/FT ³)	000000
00100	83*	C	SERR	- STANDARD ERROR OF THE SLOPE	000000
00100	84*	C	SIGMA	- STANDARD DIVIATION SIGMA	000000
00100	85*	C	SLOPE	- LEAST SQUARE SLOPE OR HEATING RATE	000000
00100	86*	C	STATME	- START TIME FOR CURVE FIT	000000
00100	87*	C	SUM1	- SUM X(I)*Y(I)	000000
00100	88*	C	SUM2	- SUM X(I)	000000
00100	89*	C	SUM3	- SUM Y(I)	000000
00100	90*	C	SUM4	- SUM (X(I)) ²	000000

00100	91•	C	SUM5 - SUM (Y(1)*2)	000000
00100	92•	C	SUM6 = (SUM X(I))10•2	000000
00100	93•	C	SUM7 = SUM X(I) * SUM Y(I)	000000
00100	94•	C	SUM8 = NPT * SUM4 - SUM6	000000
00100	95•	C	TEMP - TEMP(,1) CONTAINS SUMMED (OR AVERAGED) TEMPERATURES	000000
00100	96•	C	TEMP(,2) CONTAINS THE TEMPERATURES FOR SCAN 1	000000
00100	97•	C	TEMP(,3) CONTAINS THE TEMPERATURES FOR SCAN 2	000000
00100	98•	C	TEMP(,4) CONTAINS THE TEMPERATURES FOR SCAN NSCN = 1	000000
00100	99•	C	TEMP(,5) CONTAINS THE TEMPERATURES FOR SCAN NSCN	000000
00100	100•	C	TEMP(,6) CONTAINS THE TEMPERATURES JUST READ FROM TAPE	000000
00100	101•	C	TIM - SAVED TIMES FOR CURVE FIT	000000
00100	102•	C	TIME - TIME(1) IS THE FIRST TIME IN THE TIME SLICE	000000
00100	103•	C	TIME(2) IS THE LAST TIME IN THE TIME SLICE	000000
00100	104•	C	TIME(3) IS THE LAST TIME READ FROM TAPE	000000
00100	105•	C	TITLE1 - 1ST TITLE CARD	000000
00100	106•	C	TITLE2 - 2ND TITLE CARD	000000
00100	107•	C	TMP - SAVED TEMPERATURES FOR CURVE FIT	000000
00100	108•	C	TSTOP - COMPUTATIONAL STOP TIME	000000
00100	109•	C	TSTART - COMPUTATIONAL START TIME	000000
00100	110•	C	WORD - INPUT TEMPERATURE VALUES FOR TAB OUTPUT	000000
00100	111•	C	XX - X-COORDINATE LOCATIONS (INCHES)	000000
00100	112•	C	YDD - THE Y COORDINATES OF JUNCTION POINTS BETWEEN THE TWO	000000
00100	113•	C	THICKNESSES OF TEST MATERIAL	000000
00100	114•	C	YY - Y-COORDINATE LOCATIONS (INCHES)	000000
00100	115•	C		000000
00101	116•	C	PARAMETER NC=260,NLS=50	000000
00101	117•	C		000000
00103	118•		DIMENSION TITLE1(12), TITLE2(12), XX(50), YY(50), NTCH(50,50)	000001
00104	119•		DIMENSION TEMP(1C,6), WORD(50), QX(50,50), QY(50,50), QD0T(50,50)	000001
00105	120•		DIMENSION QD0THM(50,50), TIM(NLS), TMP(1C,NLS), ERR(50,50), DD(2)	000001
00106	121•		DIMENSION TIME(3), YDD(50)	000001
00106	122•	C		000001
00107	123•		DOUBLE PRECISION SUM1, SUM2, SUM3, SUM4, SUM5, SUM6, SUM7, SUM8	000001
00107	124•		1, SLOPE, SIGMA, SERR	000001
00107	125•	C		000001
00110	126•		DATA IBL /SH /, NTSL /D/, JEQ /3HJ /, TEOF /D/	000001
00115	127•		DATA LUIN/8/	000001
00115	128•	C		000001
00115	129•	C	INPUT SECTION	000001
00115	130•	C		000001
00115	131•	C	READ TITLE CARDS	000001
00117	132•		READ (5,1000)TITLE1	000001
00122	133•		READ (5,1000)TITLE2	000011
00125	134•		WRITE T6,2000)TITLE1,TITLE2	000021
00125	135•	C	READ CONSTANTS	000021
00131	136•		LCDERR = 0	000034
00132	137•		READ (5,1001)RHO,CP,BIGK,DD,NX,NY	000035
00142	138•		WRITE (6,2001)RHO,CP,BIGK,DD,NX,NY	000053
00152	139•		NTCLOC = NX + NY	000071
00153	140•		TF7(NTCLOC,GT+3 AND .INX*GE,3,0R*NY,GE+3),AND.NX*LE,50,AND*NY*LE+50	000074
00153	141•		.) GO TO 10	000074
00155	142•		WRITE (6,9001)	000140
00157	143•		LCDERR = 1	000145
00157	144•	C	READ TAPE INFORMATION	000145
00160	145•		10 READ(5,1002) NCHS,NCC,IOP1,NPAR,NOTH	000150
00167	146•		READ(30,1008) I	000161
00172	147•		IF(I.EQ.IBL) NPAR = 2	000167

ORIGINAL PAGE IS
OF POOR QUALITY

00174 148* IF (IOPT1.NE.0) IOPT1 = 1
00176 149* WRITE(6,2002) NCHS,NCC,IOPT1,NPAR,NOTH
00205 150* IF (NCHS-(NC-1)) 20,20,
00210 151* LCDERR = 1
00211 152* WRITE (6,4003)
00213 153* 20 CONTINUE
00214 154* IF (DD(2)) 30,30,
00217 155* READ (5,1005)(YDD(I),I=1,NX)
00225 156* WRITE (6,2019)(YDD(I),I=1,NX)
00233 157* 30 CONTINUE
00233 158* C READ X AND Y COORDINATE LOCATIONS
00234 159* READ (5,1005)(XX(I),I=1,NX)
00242 160* READ (5,1005)(YY(J),J=1,NY)
00250 161* WRITE (6,2005)(XX(I),I=1,NX)
00256 162* WRITE (6,2006)(YY(J),J=1,NY)
00256 163* C READ THERMOCOUPLE CHANNEL NUMBER AND
00256 164* C CORRESPONDING X-Y COORDINATES
00264 165* READ (5,1007)(IX,IY,NTCH(IX,IY),N=1,NTCLOC)
00274 166* WRITE(6,2007)
00276 167* WRITE(6,2022) (JEQ,J,J=1,NY)
00305 168* DO 40 I=1,NX
00310 169* WRITE (6,2008) I,(NTCH(I,J),J=1,NY)
00317 170* 40 CONTINUE
00317 171* C READ START STOP TIMES OR EVENT LEVELS
00321 172* IOPT = IOPT1 + 1
00322 173* GO TO (50,60),IOPT
00323 174* 50 READ (5,1003,END=690)TSTART,TSTOP,STATME,NTME
00331 175* IF(INTSL.GT.0) WRITE(6,2021)
00334 176* WRITE (6,2003)TSTART,TSTOP,STATME,NTME
00342 177* GO TO 70
00343 178* 60 READ (5,1004,END=690)CESTART,CESTOP,STATME,NTME
00351 179* IF(INTSL.GT.0) WRITE(6,2021)
00354 180* WRITE (6,2004)CESTART,CESTOP,STATME,NTME
00362 181* 70 IF (NTME.LE.NLS) GO TO 80
00364 182* I = NLS
00365 183* WRITE (6,4002)I
00370 184* LCDERR = 1
00371 185* 80 CONTINUE
00372 186* IF (LCDERR) ,730
00372 187* C
00372 188* C INITIALIZE AND DEFINE CONSTANTS
00372 189* C
00375 190* CON6 = RHO * CP / 24.
00376 191* CON12 = RHO * CP / 12.
00377 192* CON24 = BIGK * 24.
00400 193* IPAR = 0
00401 194* NSCN = 0
00402 195* LTEMP =((NY+9) / 10) * NX + 5
00403 196* DO 90 I=1,NCHS
00406 197* DO 90 J=2,5
00411 198* 90 TEMP(I,J) = 0.
00414 199* TESTRT = CESTART
00415 200* IESTOP = CESTOP
00416 201* NPT = 0
00417 202* LINES = 1000
00420 203* NYDD = NY + 1
00421 204* IF (DD(2)) 110,110,
000175
000201
000213
000217
000221
000227
000230
000233
000246
000261
000261
000261
000307
000321
000333
000333
000333
000345
000365
000372
000413
000413
000432
000432
000432
000435
000445
000456
000467
000500
000502
000513
000524
000536
000542
000544
000552
000555
000555
000555
000555
000555
000555
000555
000555
000555
000555
000555
000555
000555
000555
000555
000555
000573
000574
000611
000611
000611
000616
000625
000634
000635
000637
000642

00424 205* I = NY - 1 00645
 00425 206* DO 100 J = 1, 1 00650
 00430 207* IF(YY(J).LE.YDD(1),AND,YY(J+1).GT.YDD(1)) YDD = J 00654
 00432 208* 100 CONTINUE 00677
 00434 209* 110 CONTINUE 00677
 00435 210* TIME(1) = TIME(3) 00677
 00436 211* IF (NTSL-1) ,150,150 00700
 00436 212* C 00700
 00436 213* C READ INPUT TAPE 00700
 00436 214* C 00700
 00441 215* 120 READ (LUIN,ERR=130,END=140)TIME(1),(TEMP(I,6),I=1,NCHS) 00705
 00450 216* GO TO 150 00722
 00451 217* 130 WRITE (6,4004) 00724
 00453 218* GO TO 120 00730
 00454 219* 140 WRITE (6,4005)LUIN 00732
 00457 220* IEOF = 1 00737
 00460 221* GO TO 400 00741
 00461 222* 150 CONTINUE 00743
 00462 223* GO TO (160,170),IOPT 00743
 00463 224* 160 IF (TIME(1)=TSTRT) 120,190,190 00752
 00466 225* 170 IEVNT = TEMP(NCC,6) + 0.5 00757
 00467 226* IF (IEVNT-(IESTRT+2)) 180,190,120 00770
 00472 227* 180 IF (IEVNT-(IESTRT-2)) 120,190,190 00775
 00472 228* C STARTING TIME FOUND 00775
 00475 229* 190 DO 200 I=1,NCHS 001003
 00500 230* TEMP(I,1) = TEMP(I,6) 001010
 00501 231* 200 TEMP(I,2) = TEMP(I,6) 001011
 00503 232* TIME(2) = TIME(1) 001014
 00504 233* NSCN = 1 001016
 00505 234* IF(INTME.LE.2.OR.TIME(1).LT.STATME) GO TO 330 001020
 00507 235* NPT = NPT + 1 001035
 00510 236* TIM(NPT) = TIME(1) 001040
 00511 237* DO 210 I=1,NCHS 001052
 00514 238* 210 TMP(I,NPT) = TEMP(I,6) 001052
 00516 239* GO TO 330 001054
 00517 240* 220 CONTINUE 001056
 00520 241* READ (LUIN,ERR=230,END=140)TIME(3),(TEMP(I,6),I=1,NCHS) 001056
 00527 242* GO TO 240 001073
 00530 243* 230 IPAR = 1PAR + 1 001075
 00531 244* WRITE (6,4004) 001077
 00533 245* IF (IPAR-NPAR) 220,220,730 001104
 00536 246* 240 CONTINUE 001112
 00537 247* GO TO (250,260),IOPT 001112
 00540 248* 250 IF (TIME(3)=TSTOP) 280,280,400 001121
 00543 249* 260 IEVNT = TEMP(NCC,6) + .5 001126
 00544 250* IF (IEVNT-(IESTOP+2)) 270,270,280 001137
 00547 251* 270 IF (IEVNT-(IESTOP-2)) 280,400,400 001144
 00552 252* 280 TIME(2) = TIME(3) 001152
 00553 253* NSCN = NSCN + 1 001153
 00554 254* IF (NSCN>2) 300,,300 001156
 00557 255* DO 290 I=1,NCHS 001165
 00562 256* 290 TEMP(I,3) = TEMP(I,6) 001170
 00564 257* 300 CONTINUE 001170
 00565 258* DO 310 I=1,NCHS 001170
 00570 259* TEMP(I,4) = TEMP(I,5) 001175
 00571 260* TEMP(I,5) = TEMP(I,6) 001176
 00572 261* 310 TEMP(I,1) = TEMP(I,1) + TEMP(I,6) 001200

00574 262* IF(NTME.LE.2.OR.TIME(2).LT.STATME) GO TO 330 001204
 00576 263* NPT = NPT + 1 001222
 00577 264* DO 320 I=1,NCHS 001225
 00602 265* 320 TMP(I,NPT) = TEMP(I,6) 001235
 00604 266* TIM(NPT) = TIME(2) 001237
 00605 267* 330 CONTINUE 001242
 00606 268* IF(NOTH) , 365 001242
 00611 269* IF(LINES+LTEMP-55) 340,340, 001244
 00614 270* WRITE(6,2000)TITLE1,TITLE2 001251
 00620 271* LINES = 3 001264
 00621 272* 340 CONTINUE 001267
 00622 273* WRITE(6,2013)TIME(2) 001267
 00625 274* WRITE(6,2023) (JEQ,J,J=1,NY) 001303
 00634 275* LINES = LINES + LTEMP 001323
 00635 276* DO 360 I=1,NX 001335
 00640 277* DO 350 J=1,NY 001335
 00643 278* NN = NTCH(I,J) 001335
 00644 279* 350 WORD(J) = TEMP(NN,6) 001336
 00646 280* WRITE(6,2010)I,(WORD(J),J=1,NY) 001342
 00655 281* 360 CONTINUE 001363
 00657 282* 365 CONTINUE 001363
 00657 283* C 001363
 00657 284* C DO ERROR ANALYSIS IF *NTME* POINTS HAVE BEEN SAVED 001363
 00657 285* C 001363
 00660 286* IF(NTME.LE.2.OR.NPT.LT.NTME) GO TO 220 001363
 00662 287* IF(LINES+2*LTEMP-59) 370,370, 001400
 00665 288* LINES = 3 001406
 00666 289* WRITE(6,2000)TITLE1,TITLE2 001410
 00672 290* 370 WRITE(6,2015)NPT,TIM(I),TIM(NPT) 001424
 00677 291* LINES = LINES + 2 * LTEMP - 3 001435
 00700 292* CALL ERRFIT(\$395) 001442
 00700 293* C 001442
 00700 294* C OUTPUT HEATING RATE - QDOT AND PERCENT ERROR - ERR 001442
 00700 295* C 001442
 00701 296* WRITE(6,2012) 001445
 00703 297* WRITE(6,2023) (JEQ,J,J=1,NY) 001452
 00712 298* DO 380 I=1,NX 001505
 00715 299* WRITE(6,2010)I,(QDOT(I,J),J=1,NY) 001505
 00724 300* 380 CONTINUE 001524
 00726 301* WRITE(6,2016) 001524
 00730 302* WRITE(6,2023) (JEQ,J,J=1,NY) 001531
 00737 303* DO 390 I=1,NX 001552
 00742 304* WRITE(6,2010)I,(ERR(I,J),J=1,NY) 001552
 00751 305* 390 CONTINUE 001572
 00753 306* 395 CONTINUE 001572
 00754 307* TIM(I) = TIM(NPT) 001572
 00755 308* DO 396 I = 1, NCHS 001606
 00760 309* 396 TMP(I,I) = TMP(I,NPT) 001606
 00762 310* NPT = 1 001610
 00763 311* GO TO 220 001612
 00763 312* C 001612
 00763 313* C THE TIME SLICE HAS BEEN COMPLETED OR AN END OF FILE ENCOUNTERED 001612
 00763 314* C 001612
 00764 315* 400 CONTINUE 001614
 00765 316* IF(NTME.LE.2.OR.NPT.LT.3) GO TO 440 001614
 00767 317* IF(LINES+2*LTEMP-59) 410,, 001631
 00772 318* WRITE(6,2000)TITLE1,TITLE2 001637

00776	319*	410 CONTINUE	001653	
00777	320*	WRITE (6,2015)NPT,TIM(),TIM(NPT)	001653	
01004	321*	IF (NPT.LT.NTME) WRITE (6,2017)	001664	
01004	322*	C	001664	
01004	323*	C COMPUTE AND PRINT LEAST SQUARES HEATING RATE (QDOT) AND PERCENT	001664	
01004	324*	C ERROR (ERR)	001664	
01007	325*	CALL ERRFIT(\$440)	001676	
01010	326*	WRITE(6,2012)	001701	
01012	327*	WRITE(6,2023) (JEQ,J,J=1,NY)	001706	
01021	328*	DO 420 I=1,NX	001741	
01024	329*	WRITE (6,2010)I,(QDOT(I,J),J=1,NY)	001741	
01033	330*	420 CONTINUE	001760	
01035	331*	WRITE (6,2016)	001760	
01037	332*	WRITE(6,2023) (JEQ,J,J=1,NY)	001765	
01046	333*	DO 430 I=1,NX	002006	
01051	334*	WRITE (6,2010)I,(ERR(I,J),J=1,NY)	002006	
01060	335*	430 CONTINUE	002026	
01060	336*	C	002026	
01062	337*	440 CONTINUE	002026	
01063	338*	IF (NSCN=3) 680,,	002026	
01066	339*	NTSL = NTSL + 1	002031	
01067	340*	LINES = 1000	002045	
01070	341*	WRITE (6,2000)TITLE1,TITLE2	002047	
01074	342*	WRITE (6,2018)NSCN,TIME(1),TIME(2)	002064	
01101	343*	WRITE(6,2023) (JEQ,J,J=1,NY)	002074	
01110	344*	DO 460 I=1,NX	002122	
01113	345*	DO 450 J=1,NY	002122	
01116	346*	NN = NTCH(I,J)	002122	
01117	347*	TEMP(NN,1) = TEMP(NN,1) / NSCN	002123	
01120	348*	450 WORD(J) = TEMP(NN,1)	002127	
01122	349*	WRITE (6,2010)I,(WORD(J),J=1,NY)	002131	
00	01131	350*	460 CONTINUE	002155
01131	351*	C	002155	
01131	352*	C PROCESS LATERAL HEAT LOSS IN X-DIRECTION (EQUATION 3)	002155	
01131	353*	C	002155	
01133	354*	DO 470 I=1,NX	002155	
01136	355*	DO 470 J=1,NY	002155	
01141	356*	QX(I,J) = 0.	002155	
01142	357*	QY(I,J) = 0.	002155	
01143	358*	470 QDOT(I,J) = 0.	002156	
01146	359*	IF (NX-2) 530,530,	002164	
01151	360*	IDD = 1	002170	
01152	361*	DO 510 J=1,NY	002175	
01155	362*	IGOOD = 0	002175	
01156	363*	IF(J,GT,IYDD) IDD = 2	002176	
01160	364*	I1 = 0	002205	
01161	365*	480 I1 = I1 + 1	002207	
01162	366*	IF ((I1+2-NX),,510	002211	
01165	367*	NN1= NTCH(I1,J)	002215	
01166	368*	IF (NN1) 480,480,	002222	
01171	369*	I2 = I1	002224	
01172	370*	490 I2 = I2 + 1	002227	
01173	371*	IF ((I2+1-NX),,510	002231	
01176	372*	NN2 = NTCH(I2,J)	002235	
01177	373*	IF (NN2) 490,490,	002242	
01202	374*	I3 = I2	002244	
01203	375*	500 I3 = I3 + 1	002247	

OF POOR QUALITY

01204 374* IF (I3-NX) ,510 002251
 01207 377* NN3 = NTCH(I3,J) 002254
 01210 378* IF (NN3) 500,500, 002262
 01213 379* IGOOD = IGOOD + 1 002264
 01214 380* QX(I2,J) = CON24 * DD(IDD) / (XX(I3) - XX(I1)) * ((TEMP(NN2,1) -
 01214 381* TEMP(NN1,1)) / (XX(I2) - XX(I1)) - (TEMP(NN3,1)) - 002267
 01214 382* TEMP(NN2,1)) / (XX(I3) - XX(I2)) 002267
 01215 383* QX(I3,J) = QX(I2,J) 002267
 01216 384* IF (IGOOD.EQ.1) QX(I1,J) = QX(I2,J) 002322
 01220 385* IF (I3-NX) ,510,510 002337
 01223 386* NN1 = NN2 002343
 01224 387* NN2 = NN3 002345
 01225 388* I1 = I2 002347
 01226 389* I2 = I3 002351
 01227 390* GO TO 500 002353
 01230 391* 510 CONTINUE 002356
 01232 392* WRITE (6,2009) 002356
 01234 393* WRITE(6,2023) (JEQ,J=1,NY) 002363
 01243 394* DO 520 I=1,NX 002407
 01246 395* WRITE (6,2010) I,(QX(I,J),J=1,NY) 002407
 01255 396* 520 CONTINUE 002427
 01257 397* 530 CONTINUE 002427
 01257 398* C 002427
 01257 399* C PROCESS LATERAL HEAT LOSS IN Y-DIRECTION 002427
 01257 400* C 002427
 01260 401* IF (NY-2) 630,630, 002427
 01263 402* DO 610 I=1,NX 002446
 01266 403* IGOOD = 0 002446
 01267 404* IDD = 1 002447
 01270 405* J1 = 0 002451
 01271 406* 540 J1 = J1 + 1 002453
 01272 407* IF (J1+2-NY) ,610 002455
 01275 408* NN1 = NTCH(I,J1) 002461
 01276 409* IF (NN1) 540,540, 002466
 01301 410* J2 = J1 002470
 01302 411* 550 J2 = J2 + 1 002473
 01303 412* IF (J2+1-NY) ,610 002475
 01306 413* NN2 = NTCH(I,J2) 002501
 01307 414* IF (NN2) 550,550, 002506
 01312 415* J3 = J2 002510
 01313 416* 560 J3 = J3 + 1 002513
 01314 417* IF (J3-NY) ,610 002515
 01317 418* NN3 = NTCH(I,J3) 002520
 01320 419* IF (NN3) 560,560, 002525
 01323 420* IGOOD = IGOOD + 1 002527
 01324 421* IF (J2-IYDD) ,580,570 002532
 01327 422* IF (J3-IYDD) 575,575,580 002536
 01332 423* 570 IF (J2-(IYDD+1)) 590,590, 002544
 01335 424* IF (J1-IYDD) 590,590, 002550
 01340 425* IDD = 2 002554
 01341 426* 575 QY(I,J2) = CON24 * DD(IDD) / (YY(J3) - YY(J1)) * ((TEMP(NN2,1) -
 01341 427* TEMP(NN1,1)) / (YY(J2) - YY(J1)) - (TEMP(NN3,1)) - 002557
 01341 428* TEMP(NN2,1)) / (YY(J3) - YY(J2)) 002557
 01342 429* GO TO 600 002557
 01343 430* 580 YYD = YDD(I) 002612
 01344 431* QY(I,J2) = CON24 * DD(I) / (YY(J3)-YY(J1)) * ((TEMP(NN2,1) -
 01344 432* TEMP(NN1,1)) / (YY(J2)-YY(J1)) - DD(2)*(TEMP(NN3,1) - 002615

ORIGINAL PAGE IS
OF POOR QUALITY

```

01344 433*      : TEMP(NN2,1) / (DD(2)*(YYD - YY(J2)) + DD(1)*(YY(J3)
01344 434*      : - YYD))
01345 435*      GO TO 600
01346 436*      590 YYD = YDD(I)
01347 437*      QY(I,J2) = CON24 + DD(2) / (YY(J3)-YY(J1)) + (DD(1)*(TEMP(NN2,1) -
01347 438*      . TEMP(NN1,1)) / (DD(2)*(YYD - YY(J1)) + DD(1)*(YY(J2) -
01347 439*      . YYD)) - (TEMP(NN3,1) - TEMP(NN2,1)) / (YY(J3)-YY(J2)))
01350 440*      600 QY(I,J3) = QY(I,J2)
01351 441*      IF (IGOOD.EQ.1) QY(I,J1) = QY(I,J2)
01353 442*      IF (J3-NY),610,610
01356 443*      NN1 = NN2
01357 444*      NN2 = NN3
01360 445*      J1 = J2
01361 446*      J2 = J3
01362 447*      GO TO 560
01363 448*      610 CONTINUE
01365 449*      WRITE (6,20111)
01367 450*      WRITE(6,20231) (JEQ,J=1,NY)
01376 451*      DO 620 I=1,NX
01401 452*      WRITE (6,20101), (QY(I,J),J=1,NY)
01410 453*      620 CONTINUE
01412 454*      630 CONTINUE
01412 455*      C
01412 456*      C COMPUTE Q (ARRAY ERR IS USED) IF QX AND QY NOT BOTH ZERO
01412 457*      C
01413 458*      FAC = CON6 / (TIME(2) - TIME(1)) * (NSCN-1) / (NSCN-2)
01414 459*      DO 650 I=1,NX
01417 460*      IDD = 1
01420 461*      DO 650 J=1,NY
01423 462*      IF (J.GT.IYDD) IDD = 2
01425 463*      NN = NTCH(I,J)
01426 464*      ERR(I,J) = 0.
01427 465*      IF (NN) 650,650,
01432 466*      ERR(I,J) = FAC + DD(IDD) * (TEMP(NN,5) + TEMP(NN,4) - TEMP(NN,2) -
01432 467*      . TEMP(NN,3))
01433 468*      IF (QX(I,J)) 640,,640
01436 469*      IF (QY(I,J)) 640,650,640
01441 470*      640 CONTINUE
01442 471*      QDOT(I,J) = ERR(I,J) + QX(I,J) + QY(I,J)
01443 472*      QDOTMH(I,J) = QDOTMH(I,J) + QDOT(I,J)
01444 473*      650 CONTINUE
01447 474*      WRITE (6,20114)
01451 475*      WRITE(6,20231) (JEQ,J=1,NY)
01460 476*      DO 660 I=1,NX
01463 477*      WRITE (6,20101), (ERR(I,J),J=1,NY)
01472 478*      660 CONTINUE
01474 479*      WRITE (6,20121)
01476 480*      WRITE(6,20231) (JEQ,J=1,NY)
01505 481*      DO 670 I=1,NX
01510 482*      WRITE (6,20101), (QDOT(I,J),J=1,NY)
01517 483*      670 CONTINUE
01521 484*      680 IF (TEOF),,690
01524 485*      GO TO (50,60),IOPT
01524 486*      C
01524 487*      C COMPUTE AND PRINT MEANS OF MEAN HEATING RATES.
01524 488*      C
01525 489*      690 CONTINUE

```

01526 490* WRITE (6,2000)TITLE1,TITLE2 003270
 01532 491* WRITE (6,2020)NTSL 003302
 01535 492* WRITE(6,2023) (JEQ,J=1,NY) 003317
 01544 493* IF (NTSL) 730,730, 003337
 01547 494* DO 710 I=1,NX 003342
 01552 495* DO 700 J=1,NY 003354
 01555 496* 700 QDOTMM(I,J) = QDOTMM(I,J) / NTSL 003354
 01557 497* WRITE (6,2010)I,(QDOTMM(I,J),J=1,NY) 003357
 01566 498* 710 CONTINUE 003401
 01570 499* 720 CALL EXIT 003401
 01570 500* C 003401
 01571 501* 730 CALL CMERR 003404
 01571 502* C 003404
 01571 503* C FORMAT STATEMENTS 003404
 01571 504* C 003404
 01572 505* 1000 FORMAT (12A6) 003407
 01573 506* 1001 FORMAT (SF10.3,213) 003407
 01574 507* 1002 FORMAT (7I5) 003407
 01575 508* 1003 FORMAT (3F10.3,15) 003407
 01576 509* 1004 FORMAT (2F10.0,F10.3,15) 003407
 01577 510* 1005 FORMAT (SF10.3) 003407
 01600 511* 1007 FORMAT (5(2I3,I4)) 003407
 01601 512* 1008 FORMAT (15X,A5) 003407
 01602 513* 2000 FORMAT (1H1/16X,12A6/16X,12A6) 003407
 01603 514* 2001 FORMAT (IHO,15X,'MASS DENSITY OF TEST MATERIAL (RHO) ='',F12.4 003407
 01603 515* ,5X,'SPECIFIC HEAT OF TEST MATERIAL (CP) ='',F12.4 003407
 01603 516* ,/ 16X,'THERMAL CONDUCTIVITY (BIGK) ='',F12.4 003407
 01603 517* ,5X,'THICKNESS OF TEST MATERIAL (DD1) ='',F12.4 003407
 01603 518* ,/ 16X,'THICKNESS OF TEST MATERIAL (DD2) ='',F12.4 003407
 01603 519* ,5X,'NUMBER OF X-COORDINATES (NX) ='',I12 003407
 01603 520* ,/ 16X,'NUMBER OF Y-COORDINATES (NY) ='',I12 003407
 01603 521* ,/)
 01604 522* 2002 FORMAT(16X,'NUMBER OF CHANNELS ON TAPE (NCHS) ='',I12 003407
 01604 523* ,5X,'COMMAND CHANNEL NUMBER (NCC) ='',I12 003407
 01604 524* ,/ 16X,'TIME INTERVAL OR EVENT CODE (IOPT1) ='',I12 003407
 01604 525* ,5X,'ACCEPTABLE NO. OF PARITIES (NPAR) ='',I12 003407
 01604 526* ,/ 16X,'TIME HISTORY TAB OPTION (NOTH) ='',I12 003407
 01604 527* ,/)
 01605 528* 2003 FORMAT(IHO,15X,'START TIME ='',F10.3,' STOP TIME ='',F10.3 / 003407
 01605 529* ,16X,'LEAST SQUARES START TIME ='',F10.3,' NO OF POINTS FOR ', 003407
 01605 530* ,,'LEAST SQUARES COMPUTATIONS (NTME1) ='',I10) 003407
 01606 531* 2004 FORMAT(IHO,15X,'COMMAND EVENT START LEVEL ='',F12.4,5X,'STOP LEVEL' 003407
 01606 532* ,'' ='',F12.4/ 003407
 01606 533* ,16X,'LEAST SQUARES START TIME ='',F10.3,' NO OF POINTS FOR ', 003407
 01606 534* ,,'LEAST SQUARES COMPUTATIONS (NTME1) ='',I10) 003407
 01607 535* 2005 FORMAT (IHO,15X,'X-COORDINATES ...'/(2IX,10F10.3)) 003407
 01610 536* 2006 FORMAT (IHO,15X,'Y-COORDINATES ...'/(2IX,10F10.3)) 003407
 01611 537* 2007 FORMAT (IHO,15X,'INPUT TAPE CHANNEL NUMBERS ...') 003407
 01612 538* 2008 FORMAT (1H ,15X,'1 ='',I2,10F10.(/22X,10F10.)) 003407
 01613 539* 2009 FORMAT(IHO,10X,'MEAN LATERAL HEAT LOSS IN X-DIRECTION ...') 003407
 01614 540* 2010 FORMAT (1H ,5X,'1 ='',I3,10F10.3/(12X,10F10.3/)) 003407
 01615 541* 2011 FORMAT(IHO,10X,'MEAN LATERAL HEAT LOSS IN Y-DIRECTION ...') 003407
 01616 542* 2012 FORMAT(IHO,10X,'MEAN HEATING RATE ...') 003407
 01617 543* 2013 FORMAT (IHO,10X,'TIME ='',F10.3?/IX,'CURRENT TEMPERATURE ...') 003407
 01620 544* 2014 FORMAT(IHO,10X,'MEAN HEAT FLUX WITHOUT CONDUCTION CORRECTION ...') 003407
 01621 545* 2015 FORMAT (IHO,10X,'LINEAR CURVE FIT USING ''I3,' POINTS. TIME ='', 003407
 01621 546* ,F10.3,' TO'',F10.3,' SEC') 003407

01622	547•	2016 FORMAT(IHO,10X,'PERCENT STANDARD ERROR . . .')	003407
01623	548•	2017 FORMAT(IH4,TB9,T000 FEWER POINTS THAN REQUESTED 6.67)	003407
01624	549•	2018 FORMAT(IHO,10X,'TEMPERATURES AVERAGED OVER',I5,', POINTS. TIME IN'	003407
01624	550•	.,'INTERVAL PROCESSED',F10.3,', T00,F10.3,', SEC')	003407
01625	551•	2019 FORMAT(IHO,15X,'Y-COORDINATES OF THICKNESS DIFFERENCE JUNCTION...')	003407
01625	552•	.(1/2IX,T0F10.3))	003407
01626	553•	2020 FORMAT(IHO,10X,'MEANS OF MEAN HEATING RATES FOR',I3,', TIME PERIOD'	003407
01626	554•	.,'S....')	003407
01627	555•	2021 FORMAT(IH1)	003407
01630	556•	2022 FORMAT	003407
01630	557•	.(2BX,A3,I2,5X,A3,I2,5X,A3,I2,5X,A3,I2,5X,A3,I2,5X,A3,I2,	003407
01630	558•	.5X,A3,I2,5X,A3,I2,5X,A3,I2,	003407
01631	559•	2023 FORMAT	003407
01631	560•	.(17X,A3,I2,5X,A3,I2,5X,A3,I2,5X,A3,I2,5X,A3,I2,5X,A3,I2,	003407
01631	561•	.5X,A3,I2,5X,A3,I2,5X,A3,I2,	003407
01632	562•	4001 FORMAT(IX,'*** ERROR - NX OR NY IS BAD')	003407
01633	563•	4002 FORMAT(IX,'*** ERROR - NTME IS LARGER THAN ',I3)	003407
01634	564•	4003 FORMAT(IX,'*** ERROR - TOO MANY CHANNELS')	003407
01635	565•	4004 FORMAT(IHO,10X,'* * * PARITY ERROR RECORD DELETED * * *)	003407
01636	566•	4005 FORMAT(IHO,10X,'END OF FILE ENCOUNTERED ON UNIT ',I2,' PROCESSING'	003407
01636	567•	.* OF ACCUMULATED DATA WILL BE ATTEMPTED.')	003407
01636	568•	C	003407
01636	569•	C*****	003407
01636	570•	C*****	003407
01636	571•	C	003407
01637	572•	SUBROUTINE ERRFIT(S)	003407
01637	573•	C	003407
5	574•	C SUBROUTINE TO COMPUTE THE HEATING RATE BY FITTING A GIVEN TIME	003407
01637	575•	INTERVAL OF DATA TO A FIRST DEGREE POLYNOMIAL AND TO COMPUTE	003407
01637	576•	THE STANDARD AND PERCENT ERROR OF THIS HEATING RATE.	003407
01637	577•	C	003407
01642	578•	IF (NPT.LE.2) GO TO 999	003407
01642	579•	C	003407
01644	580•	SUM2 = 0.0	003407
01645	581•	4 SUM4 = 0.0	003414
01646	582•	DO 125 M = I,NPT	003446
01646	583•	C SUM X(I)	003446
01651	584•	SUM2 = SUM2 + TIM(M)	003446
01651	585•	C SUM (X(I))**2	003446
01652	586•	SUM4 = SUM4 + TIM(M)**2	003451
01653	587•	125 CONTINUE	003456
01653	588•	C (SUM X(I))**2	003456
01655	589•	SUM6 = SUM2**2	003456
01655	590•	SUM8 = NPT * SUM4 - SUM6	003460
01656	591•	C	003460
01657	592•	DO 200 I = I,NX	003464
01662	593•	DO 200 J = I,NY	003513
01665	594•	IDD = 1	003513
01666	595•	IF(J.GT.IYDD) IDD = 2	003515
01670	596•	NN = NTCHIT,J)	003524
01671	597•	IF (NN.LE.0) GO TO 175	003526
01673	598•	SUM1 = 0.0	003532
01674	599•	SUM3 = 0.0	003534
01675	600•	SUM5 = 0.0	003535
01676	601•	DO 150 M = I,NPT	003545
01676	602•	C SUM Y(I)*Y(I)	003545
01701	603•	SUM1 = SUM1 + TIM(M) * TMP(NN,M)	003545

01701 604* C SUM Y(I)
 01702 605* SUM3 = SUM3 + TMP(NN,M)
 01702 606* C SUM (Y(I)**2)
 01703 607* SUM5 = SUM5 + TMP(NN,M)**2
 01704 608* 150 CONTINUE
 01704 609* C SUM X(I) = SUM Y(I)
 01705 610* SUM7 = SUM2 + SUM3
 01706 611* C SLOPE
 01707 612* SLOPE = (NPT * SUM1 - SUM7) / SUM8
 01707 613* C SIGMA
 01710 614* SIGMA = 1.0 / NPT * SQRT(NPT * SUM5 - SUM3**2)
 01710 615* I - (NPT * SUM1 - SUM7)**2 / SUM8
 01710 616* C STANDARD ERROR
 01711 617* SERR = NPT * SIGMA / SQRT((NPT-2) * SUM8)
 01711 618* C PERCENT ERROR
 01712 619* ERR(I,J) = SERR / SLOPE * 100.0
 01712 620* C HEATING RATE
 01713 621* QDOT(I,J) = CON12 * DD(1DD) * SLOPE
 01714 622* GO TO 200
 01715 623* 175 ERR(I,J) = 0.0
 01716 624* QDOT(I,J) = 0.0
 01717 625* 200 CONTINUE
 01722 626* RETURN
 01722 627* C
 01723 628* 999 WRITE (6,9999)
 01725 629* 9999 FORMAT (IHO,10X,'TOO FEW POINTS AVAILABLE FOR CURVE FIT.')
 01726 630* RETURN
 01726 631* C
 01727 632* END

END OF COMPILATION: NO DIAGNOSTICS.

SCOPOUT TPF5., THNSKN.
 FURPUR 0026-12/20-03:02
 1 SYM 1 REL
 SPREP

ORIGINAL PAGE IS
OF POOR QUALITY

ATTACHMENT 6

SAMPLE INPUT

(TO BE SUPPLIED LATER)

ATTACHMENT 7

SAMPLE OUTPUT

(TO BE SUPPLIED LATER)

ATTACHMENT 8

CORRESPONDENCE

014 017 PROGRAM NO
JSC Q614

JSC COMPUTER PROGRAM ABSTRACT

0114 DATE (MMDDYY)

1-21-75

0120 TITLE OF PROGRAM (62 CHARACTERS MAXIMUM) SURFACE HEATING RATE OF THIN SKIN MODELS				0172 SYMBOLIC NAME (9 CHARACTERS MAXIMUM) THNSKN	PARENT PROGRAM 0214 CATEGORY 0216 SITE 0219 PROGRAM NO		
0226 CATEGORY <input type="checkbox"/> FOR V	0227 LANGUAGE NO. 1	0232 LANGUAGE NO. 2	0237 KEY WORDS (8 MAXIMUM SEPARATED BY COMMAS) Arc Jet, Heat Rate, Thin Skin, Thermocouples				
WHOM TO CONTACT ABOUT THE PROGRAM					0548 STATUS		0549
0514 CONTACT (LAST NAME) Stephenson	0528 SITE JSC	0531 ORGN CODE FD57	0539 PROJECT NO 4300	0545 NASA CENTER	<input type="checkbox"/> A. UNDER DEVELOPMENT <input type="checkbox"/> B. OPERATIONAL <input checked="" type="checkbox"/> C. COMPLETED	A. THIS PROGRAM IS NOT FOR SHARING <input type="checkbox"/> B. LIMITED SHARING (SEE ABSTRACT) <input type="checkbox"/>	
DATES		0558 REVISION CODE		TIME AND COST FOR DEVELOPMENT			
0550 INITIATED MMYY 11-74	0554 COMPLETED MMYY 12-74	<input checked="" type="checkbox"/> A. REVISION <input type="checkbox"/> B. CANCELLATION		0559 MAN-MONTHS 8	0564 MACHINE HOURS 2 0	0569 COMPUTER TYPE 1108	0574 TOTAL COST (DOLLARS) 74 75 76 77 78 79 80
59 60 61 62 63	64 65 66 67 68			ELITE MARGIN PICA MARGIN			
CARD NUMBER 2410	ABSTRACT						
06	THNSKN computes the mean heating rate at up to 100 locations on the surface of thin skin transient heating rate models. Output is printed in tabular form and consists of time history tabulation of temperatures, average temperatures, heat loss without conduction correction, mean heating rate, least squares heating rate, and the percent standard error of the least squares heating rates. The input tape used is produced by the program EHTS03. (SCR 83-15-30/McBryde)						
16							
17							
18							
19							
20							
21							
22							
23							
24							
25							
26							
27							
28							
29							
30							
31							
32							
33							
34							
35							
36							
37							
38							
39							
40							
41							
RELATED DOCUMENTATION (66 CHARACTERS MAXIMUM SEPARATE EACH REF BY COMMAS)							
42							

UNITED STATES GOVERNMENT

Memorandum

Computation and Analysis Division
NASA Manned Spacecraft Center
Houston, Texas 77058

TO : LEC/Manager, Test Data Reduction
Department, 672-10

DATE: October 27, 1969

FROM : ED5/Acting Chief, Data Processing Branch

In reply refer to:
11-69-622

SUBJECT: Requirements for a Thin Skin Transient Heating Rate Model
Program

Programming support is required to develop a program to compute heating rates of thin skin transient heating rate models. This program will be developed for the Experimental Heat Transfer Section of the Structures and Mechanics Division. The program will be used to support definition of the aerothermodynamic design of the MSC space shuttle vehicle.

It is necessary that the program, specified by the attached requirements document, be operation by October 31, 1969. Preliminary requirements have been reviewed by Dr. Carl D. Scott, project engineer, and forwarded to Mrs. Yvonne Chempinski. Work on this task should be charged to project number 4556. For further information, please contact Mr. E. O. Grice, extension 5533.



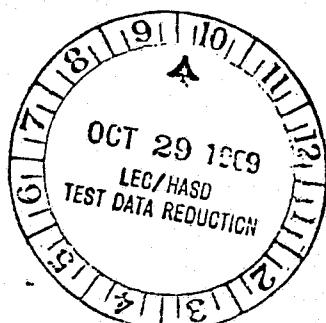
Fred Fulton

Enclosure

cc:

ES56/Dr. C. D. Scott

ED57:EOGrice(LEC:JMRandall):ddc 10-27-69



DATA PROCESSING REQUIREMENTS
for a
THIN SKIN TRANSIENT HEATING RATE MODEL PROGRAM

Prepared by:

J. M. Randal
J. M. Randal 22 Oct 69
LEC Requirements & Analysis

Approved by:

K. J. Langenberg
K. J. Langenberg 10-24
LEC Requirements & Analysis

Concurrence by:

E. O. Grice
E. O. Grice 10/23/69
CAD Requirements & Analysis

Concurrence by:

Carl D. Scott
Carl D. Scott 10/22/69
Experimental Heat Transfer Section

PROJECT DISCUSSION

The Experimental Heat Transfer Section of the Structures and Mechanics Division has requirements for a digital computer program to compute heating rates of thin skin transient heating rate models. These models will be tested in either the 1.5 Megawatt or the 10 Megawatt Arc-Heater facility. The tests in which such models will be used will be directly related to current MSC space shuttle vehicle activities. The program outputs will be used to support definition of the aerothermodynamic design of the MSC space shuttle vehicle configuration.

TEST CONFIGURATION

The thin skin transient heating rate models will be constructed with a thin metal skin. Thermocouple instrumentation will be attached to the back side of the skin in rectangular arrays and used to measure temperature. When these models are subjected to a non-uniform constant heat flux by the arc-heater equipment, the surface temperature of the skin will increase according to the laws of heat conduction and capacitance. The skin will be sufficiently thin so that the temperature gradient normal to the skin will be negligible. Therefore, it will be assumed that the thermocouples attached to the back surface actually measure the temperature of the skin at each location.

The analog signals output by the thermocouple array will be digitized by use of either the 160 channel data acquisition system located in Building 222 or the 50 channel data acquisition located in Building 262. The digital data tape output by either of these systems will be compatible with the CAD UNIVAC 1108 digital computer system. The existing EHTS03 (Q566) program will be used to calibrate the experimental data in engineering units and output a data tape for input to the required thin skin transient heating rate model program. See Figure 1 for a diagram of the data flow and test configuration.

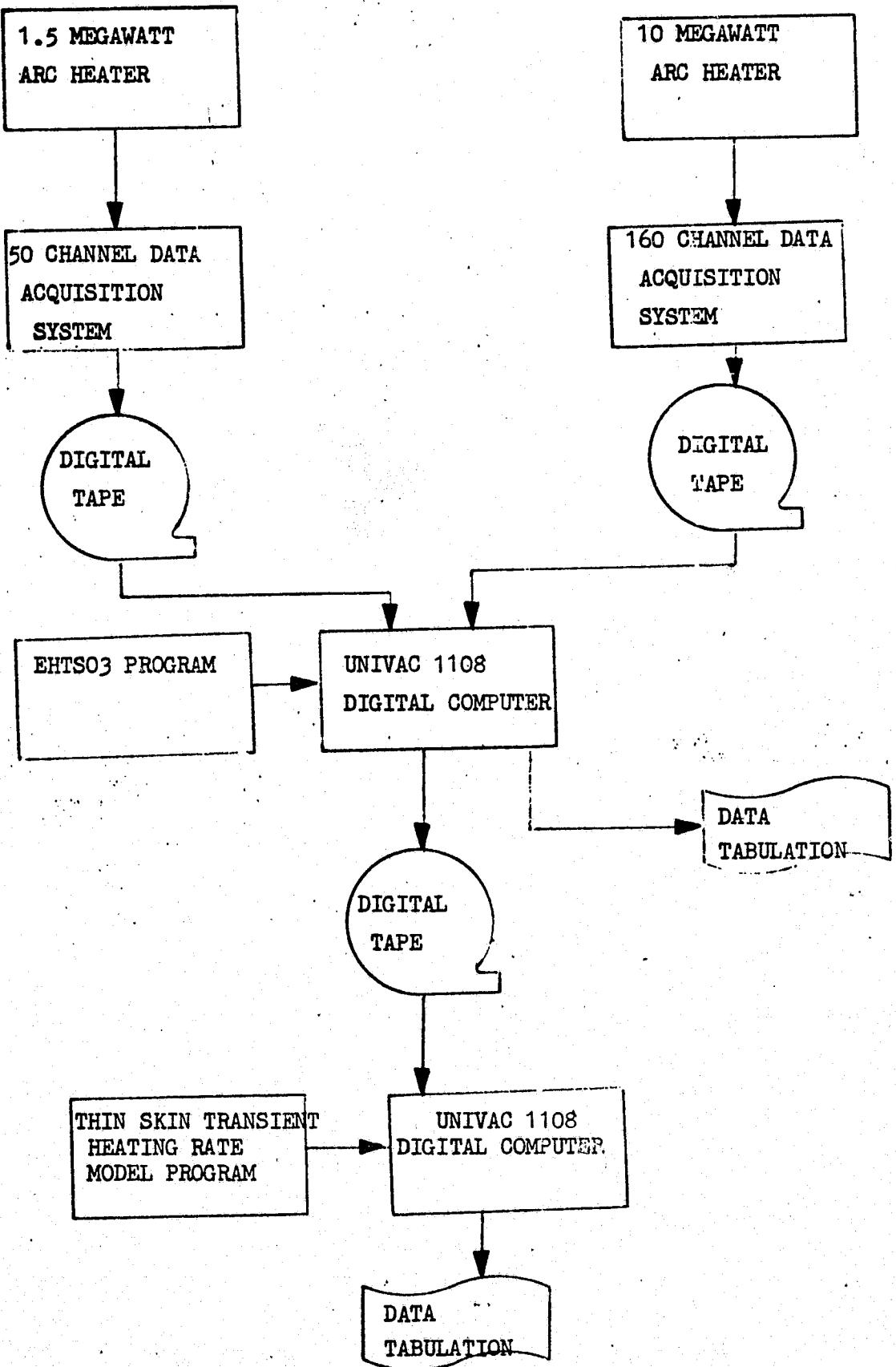


Figure 1
TEST CONFIGURATION

III

DATA PROCESSING REQUIREMENTS

The hardware required to accomplish the data processing task will be the UNIVAC 1108 digital computer. The software required will be the existing EHTS03 (Q566) program and the Thin Skin Transient Heating Rate Model Program specified in Appendix A.

The data processing procedure will consist of the steps listed below:

1. The project engineer will have the data tape and the lead card input for the EHTS03 program delivered to the test data coordinator in Room 228 of Building 12.
2. The data coordinator will issue instructions for computer processing and notify the project engineer when the processing is complete.
3. The project engineer will review the EHTS03 data and provide lead card setups for the thin skin transient heating rate model program.
4. The data coordinator will issue instructions for computer processing and notify the project engineer when the processing is complete.

IV

TECHNICAL REFERENCES

1. Memo: ES5/9-24(9)/249M, Memorandum to: ED/Chief, Computation and Analysis Division; from: ES/Chief, Structures and Mechanics Division; Subject: Requirements for a computer program to calculate heating rates using thin skin models.
2. Program Documentation, Experimental Heat Transfer Data Reduction Package #3 (EHTS03), Program Q566, Project 4556, August 1969.

APPENDIX A
PROGRAMMING SPECIFICATION
for
THIN SKIN TRANSIENT HEATING RATE MODEL PROGRAM

I

PURPOSE

The purpose of this program will be to compute the heating rate at each of a number of locations on the surface of thin skin transient heating rate models. Experimental data, calibrated in engineering units, will be obtained from the ABEL tape output by the EHTS03 computer program. The program output will consist of time history tabulations of computed data with options for input and intermediate computation tabulations.

II

INPUT

The program inputs will be the ABEL time history data tape output by the EHTS03 program and the lead card inputs necessary to specify computational constants, input data channels, command channels, options, and command event levels. The magnetic input data tape will consist of FORTRAN written data records in a single data file. The first data word in each record will be the time word. The remaining words will be the data channel words ordered by channel number. The tape will be written with 800 bit per inch density and odd parity using the UNIVAC 1108 computer.

The lead card inputs will include, but not be limited to, the following items. The exact card formats will be determined by the programmer.

1. Two cards, each containing at least sixty column alphanumeric entries will be used to identify the data contained in the output tabulation. This input will appear in the title of each page of the tabulation.

2. Coordinate positions for each thermocouple with a maximum array of 50x50 positions. The upper left hand position will be designated $T_{xy} = T_{11}$ as shown by Table 1 in Section III.
3. Input tape data channel number for each thermocouple in T_{xy} array.
4. Physical locations of each row and column. All locations will be determined from the row and column containing $T_{xy} = T_{11}$ in inches.
5. Input tape data channel number for the command channel.
6. Command channel signal level used to start computations. Millivolt level.
7. Command channel signal level used to terminate computations. Millivolt level.
8. Input tape data channel number for the time channel. Normally channel 1.
9. Start computation time.
10. Stop computation time.
11. Coordinate positions of known erroneous thermocouple data.
12. Option to tabulate tape input temperatures.
13. Option to tabulate intermediate computation results.

14. Computational constants:

- a. Mass density (ρ) of the test material in pounds mass per cubic foot. (lbm/ft^3)
- b. Specific heat (c_p) of the test material in $\text{Btu}/\text{lbm}^{\circ}\text{F}$
- c. Material thickness (d) in inches
- d. Thermal conductivity (K) in $\text{Btu}/\text{ft sec}^{\circ}\text{F}$

III

TABLES

The thermocouple instrumentation used to measure the temperatures on the thin skin transient heating model will be arrayed in the rectangular coordinate system shown by Table 1. The maximum size of the array will be 50x50. The minimum array will be 3x1 or 1x3. Only line, rectangular or square arrays will be defined. Other array configurations may be computed if dummy data is input to fill out the array. Even though the thermocouple array will generally be rectangular, the spacing between rows and columns will not normally be the same. Therefore, the distance of each row and column from $T_{1,1}$ will be a separate card input. The array will be computed as for a planar surface regardless of the actual configuration of the model. That is, the last row will not be adjacent to the first row as in the case of a cylindrical surface, etc. Spherical and conical surfaces will not be defined other than as rectangular arrays.

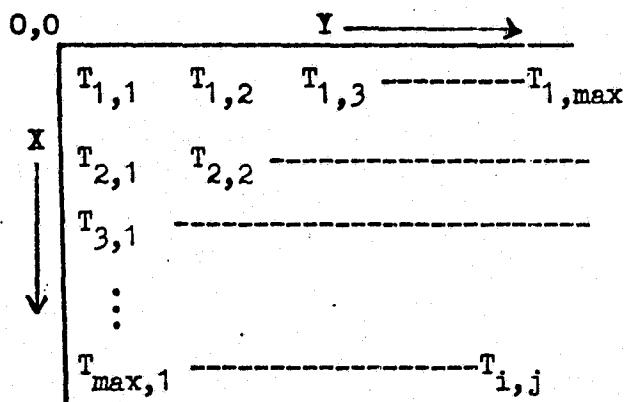


TABLE 1

THERMOCOUPLE ARRAY

IV

COMPUTATIONS

Equation 1 will be the energy balance equation used to describe the heating applied to the model surface at each coordinate (x_i, y_j) for each data time sample (t_k).

Equation 1:

$$\dot{q}_{ij} = \left(\frac{\rho_d C_p}{12} \right) \left(\frac{\partial T_{ij}}{\partial t} \right) + \left(\dot{q}_{ij}^x \right) + \left(\dot{q}_{ij}^y \right)$$

where:

\dot{q}_{ij} : Heating rate to the model surface x_i, y_j

ρ : Mass density of surface material

d : Material thickness of surface material

C_p : Specific heat of surface material

$\left(\frac{\partial T_{ij}}{\partial t} \right)$: Derivative computed by the use of equation 2

$\left(\dot{q}_{ij}^x \right)$: Derivative computed by the use of equation 4

$\left(\dot{q}_{ij}^y \right)$: Derivative computed by the use of equation 5

Equation 2 will be used to compute the partial derivative of temperature with respect to time for the thermal mass around the thermocouple test point for each data time sample (t_k).

Equation 2:

$$\frac{\partial T_{ij}}{\partial t} = b_k + 2c_k t_k$$

Where:

b_k : Determined by solution of equations 3a, 3b, and 3c

c_k : Determined by solution of equations 3a, 3b and 3c

Equations 3a, 3b and 3c will be solved for b_k and c_k by the use of the Gauss-Jordan or other appropriate method for the solution of simultaneous equations.

$$T_{ij}(t_{k-1}) = a_k + b_k t_{k-1} + c_k (t_{k-1})^2$$

$$T_{ij}(t_k) = a_k + b_k t_k + c_k (t_k)^2$$

$$T_{ij}(t_{k+1}) = a_k + b_k t_{k+1} + c_k (t_{k+1})^2$$

Where:

a_k, b_k, c_k : Coefficients of a second degree polynomial

t_{k-1} : Time of preceding data sample from ABEL input tape

t_k : Time of current data sample

t_{k+1} : Time of succeeding data sample

Equation 4 will be used to compute the lateral heat loss in the X direction for input to equation 1 for each time sample (t_k).

Equation 4:

$$\dot{q}_{ij}^x = 24 \text{ kd} \left[\left(\frac{1}{x_{i+1} - x_{i-1}} \right) \left(\frac{T_{ij} - T_{i-1,j}}{x_i - x_{i-1}} + \frac{T_{i+1,j} - T_{ij}}{x_{i+1} - x_i} \right) \right]$$

Where:

k : Thermal conductivity (card input)

d : Material thickness (card input)

$x_{i+1} - x_{i-1}$: Distance between thermocouples located on either side of x_i thermocouple, etc.

$T_{ij} - T_{i-1,j}$: Input data temperature difference between thermocouples.

Equation 5 will be used in the same manner as equation 4 to determine the lateral heat loss in the Y direction for each data time sample.

Equation 5:

$$\dot{q}_{ij}^y = 24 \text{ kd} \left[\left(\frac{1}{y_{j+1} - y_{j-1}} \right) \left(\frac{T_{ij} - T_{i,j-1}}{y_j - y_{j-1}} + \frac{T_{i,j+1} - T_{ij}}{y_{j+1} - y_j} \right) \right]$$

Equation 1 will be set to zero for the two end points in a test array consisting of a single line of thermocouples. Further, equation 1 will be set to zero for the four corner transducers in a square or rectangular array. That is:

$$2 \leq i \leq I-1,$$

$$2 \leq j \leq J-1$$

where: I and J are defined as the greatest i and j limits, respectively, of the transducer array.

Equation 1 will be computed for the test points in the transducer array that lie on the four sides of 3x2, 2x3 or larger arrays. Either equation 4 or equation 5 will be modified as required to prevent erroneous results due to lack of valid inputs for the transducers located on the sides of the test array. For test points located on the upper side of the test point array, equation 6 will be used instead of equation 4.

Equation 6:

$$q_{ij} = 24 \text{ kd} \left(\frac{2}{X_2 - X_1} \right) \left(\frac{T_{2j} - T_{ij}}{X_2 - X_1} \right)$$

For test points located in the lower side of the array, equation 7 will be used in lieu of equation 4.

Equation 7:

$$\dot{q}_{Ij}^x = 24 \text{ kd} \left(\frac{2}{x_I - x_{I-1}} \right) \left(\frac{T_{Ij} - T_{I-1,j}}{x_I - x_{I-1}} \right)$$

Equation 5 will be valid regardless of whether equations 6 or 7 are used for upper and lower limit test points.

For test points located on the left side of the array shown in Table 1, equation 8 will be used in lieu of equation 5.

Equation 8:

$$\dot{q}_{i1}^y = 24 \text{ kd} \left(\frac{2}{y_2 - y_1} \right) \left(\frac{T_{i2} - T_{i1}}{y_2 - y_1} \right)$$

For test points located on the right side of the array, equation 9 will be used in lieu of equation 5.

Equation 9:

$$\dot{q}_{ij}^y = 24 \text{ kd} \left(\frac{2}{y_j - y_{j-1}} \right) \left(\frac{T_{i,j} - T_{i,j-1}}{y_j - y_{j-1}} \right)$$

Equation 4 will be valid regardless of whether equations 8 or 9 are used for left or right test points. Note that the end points of a linear array and corner points of a rectangular array will not be computed, as previously stated.

Card input will be used to specify which if any, of the input test points have invalid tape data input due to hardware malfunction in the test hardware or the data acquisition system. Computations for the test points on the four sides of the invalid points will be made by using the input temperature from and the distance to the thermocouple on the opposite side of the faulty point. For example, if $T_{2,2}$ were faulty (see Table 1), $\dot{q}_{2,1}^Y$ would be computed using $T_{2,3}$ for the temperature input and $Y_3 - Y_1$ for the distance input to equation 5. Note that the program will be designed to salvage data only for points within the array. A bad point at any edge or corner of the array will be eliminated by deleting that row or column from the program input. Substitution of data from a similar point may also be done by card input. No provision will be made for computing data around specified bad input points that are separated by at least one row or column of good input data.

Computations will be controlled by card input start-stop times or by card input command channel levels. Either one or the other may be used, but not both. Start-stop times will be input in seconds and milliseconds. Command Channel start and stop levels will be input at the same levels used in the ETHS03 program. These levels will be 30, 35, 40, 45, 50, 55, 60, 65, 70, 75, 80, 85, 90 and 95 millivolts plus or minus 2.5 millivolts.

PROGRAM OUTPUT

The program output will consist of tabulations of the input lead cards, thermocouple array format, computed and input data. No data tape will be output. Each page of the tabulated output will be identified by the card input identification title in addition to any other identification, column headings, etc. The tabulations will include:

1. Tabulation of all input card data.
2. Row by row tabulation of input tape data channels: This tabulation will start with the channel number for $T_{xy} = T_{11}$ and list the input data channels in 10 columns across the page. See Table 1 for a typical format. Channel numbers assigned will be set to zero for those channels specified as erroneous by card input.
3. Row by row tabulation of computed heating rate (\dot{q}_{ij}) for each time history slice. The time of each sample will precede each beginning row of computed data. Time will be output in seconds and milliseconds.
4. Optional row by row tabulation of tape input data temperatures for each time history slice as tabulated in 3, above.
5. Optional row by row tabulation of computed X and Y heat losses (\dot{q}_{ij}^X and \dot{q}_{ij}^Y) as in 3, above.

Note that tabulated data outputs for non-computed end points, corner points and bad data points will set to zero.



LOCKHEED ELECTRONICS COMPANY

HOUSTON AEROSPACE SYSTEMS
16811 EL CAMINO REAL
HOUSTON, TEXAS 77058
TELEPHONE: (AREA CODE 713) 488-0080

In reply refer to:
TDR#2247

October 31, 1969

TO: ED5/Chief, Data Processing Branch
FROM: LEC/Manager, Test Data Reduction Department
SUBJECT: Technical Memorandum 11-69-622, October 27, 1969,
Requirements for a Thin Skin Transient Heating
Rate Model Program

Subject Technical Memorandum was received by the Test Data Reduction Department on October 29, 1969.

Responsibility for the requested programming support has been assigned to Mrs. Yvonne Chempinski. Mrs. Chempinski has been working from preliminary requirements documents. The program has been completed on schedule with test output delivered to Doctor Scott. Two minor additions were requested by Doctor Scott and will be completed shortly.

Please direct any additional communications regarding this project to Mrs. Chempinski at HU8-0080, extension 345 or Mr. Len Martin, ext. 336.

Unless otherwise directed, all effort expended on this task will continue to be charged to Project Number 4556.

Doyle L. Johnson
Doyle L. Johnson

DLJ:JDG:pm

Distribution: J. Fisher/ED57
E. Grice/ED57
J. Randall/C18
Y. Chempinski/B11
L. Martin/B11
D. Garrett/B11

UNITED STATES GOVERNMENT

Memorandum

Computation and Analysis Division
NASA Manned Spacecraft Center
Houston, Texas 77058

11/24

TO : LEC/Manager, Test Data Reduction Department, 672-10

DATE: November 18, 1969

FROM : ED5/Chief, Data Processing Branch

In reply refer to:
11-69-634

SUBJECT: Requirements for modification of the THNSKN (Q614) program

Programming support is required to modify the Thin Skin Transient Heating Rate Model Program. The modifications requested by Dr. C. D. Scott of the Experimental Heat Transfer Section of the Structures and Mechanics Division are listed below:

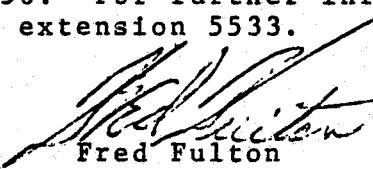
a. Change the card input format for X and Y coordinates from F 5.1 to F 10.3...

b. Change the data output print format to F 10.3.

c. Make the tabulation of tape input data temperatures, X and Y lateral heat losses as standard output rather than optional.

d. Compute end point and corner point data for the thermocouple array rather than setting this data to zero.

It is understood that Mrs. Yvonne Chempinski has started work on these modifications in response to a verbal request from Dr. Scott. Work on this task should be a continuing charge to project number 4556. For further information, please contact E. O. Grice, extension 5533.

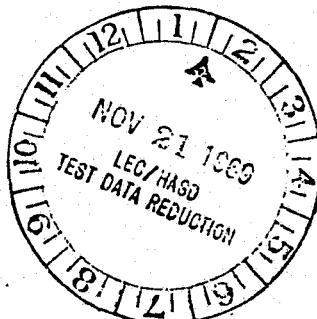


Fred Fulton

cc:

ES56/Dr. C. D. Scott
ED57/J. L. Fisher

ED57:EOGrice(LEC:JMRandall):ddc 11-18-69





LOCKHEED ELECTRONICS COMPANY

HOUSTON AEROSPACE SYSTEMS
16811 EL CAMINO REAL
HOUSTON, TEXAS 77058
TELEPHONE: (AREA CODE 713) 488-0080

In reply refer to:
TDR#2267

November 25, 1969

TO: ED5/Chief, Data Processing Branch
FROM: LEC/Manager, Test Data Reduction Department
SUBJECT: Technical Memorandum 11-69-634, November 18, 1969
Requirements for Modification of the THNSKN (Q614)
Program

Subject Technical Memorandum was received by the Test Data Reduction Department on November 21, 1969.

Responsibility for maintenance of the THNSKN program has been assigned to Mrs. Yvonne Chempinski. The program modifications specified in the subject Technical Memorandum have been completed, and the modified program has been validated.

Please direct any further communications regarding this task to Mrs. Chempinski, HU8-0080, extension 345.

As directed, all effort expended on this task will continue to be charged to Project Number 4556.

Doyle L. Johnson
Doyle L. Johnson

DLJ:JDG:pm

Distribution: J. L. Fisher/ED57
E. O. Grice/ED57
J. M. Randal/C18
Y. Chempinski/B11
J. D. Garrett/B11



NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
MANNED SPACECRAFT CENTER
HOUSTON, TEXAS 77058

IN REPLY REFER TO: 11-69-636

24 NOV 1969

TO : LEC/Manager, Test Data Reduction Department 672-10
FROM : ED5/Chief, Data Processing Branch
SUBJECT: Requirements for modification of the THNSKN (Q614) program

Programming support is required to modify the Thin Skin Transient Heating Rate Model Program. Equations 4 and 5 are to be changed to the form shown below:

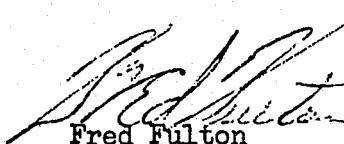
Equation 4:

$$\dot{q}_{ij}^X = 24kd \left[\left(\frac{1}{x_{i+1} - x_{i-1}} \right) \left(\frac{T_{ij} - T_{i-1,j}}{x_i - x_{i-1}} - \frac{T_{i+1,j} - T_{ij}}{x_{i+1} - x_i} \right) \right]$$

Equation 5:

$$\dot{q}_{ij}^X = 24kd \left[\left(\frac{1}{y_{j+1} - y_{j-1}} \right) \left(\frac{T_{ij} - T_{i,j-1}}{y_j - y_{j-1}} - \frac{T_{i,j+1} - T_{ij}}{y_{j+1} - y_j} \right) \right]$$

Mrs. Yvonne Chempinski has started work on these changes in response to a verbal request from Dr. Scott. Work on this task should be a continuing charge to project number 4556. For further information, please contact E. O. Grice, extension 5533.

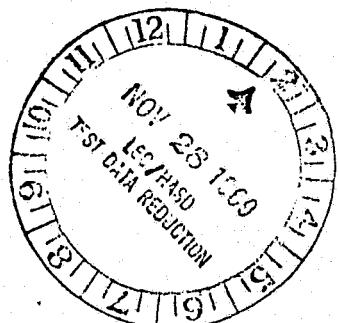


Fred Fulton

cc:

ES56:Dr. C. D. Scott

ED57/EOGrice(LEC:JMRandal):bc 11-20-69





HOUSTON AEROSPACE SYSTEMS
16811 EL CAMINO REAL
HOUSTON, TEXAS 77058
TELEPHONE: (AREA CODE 713) 488-0080

LOCKHEED ELECTRONICS

COMPANY

In reply refer to:
TDR#2272

December 1, 1969

TO: ED5/Chief, Data Processing Branch
FROM: LEC/Manager, Test Data Reduction Department
SUBJECT: Technical Memorandum 11-69-636, November 24, 1969
Requirements for Modification of the THNSKN Program
(Q614)

Subject Technical Memorandum was received by the Test Data Reduction Department on November 28, 1969.

Programming support for the subject program has been assigned to Mrs. Yvonne Chempinski of the Data Acquisition Systems programming group. Mrs. Chempinski has completed the requested program modifications having worked from a verbal request from Doctor Carl Scott.

Please direct any additional communications regarding this project to Mrs. Chempinski, HU8-0080, extension 345, or to Mr. Len Martin, the Engineering Applications Programming team leader, at extension 336.

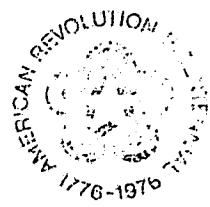
As directed, all work expended on this task will continue to be charged to Project Number 4556.

Doyle L. Johnson
Doyle L. Johnson

DLJ:JDG:pm

Distribution: J. L. Fisher/ED57
E. O. Grice/ED57
J. M. Randal/C18
Y. Chempinski/B11
L. Martin/B11
J. D. Garrett/B11

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
LYNDON B. JOHNSON SPACE CENTER
HOUSTON, TEXAS 77058



REPLY TO:
ATTN OF: ES35

December 23, 1974

Lockheed Electronics Co. Inc.
Attn: Mr. James Brose
Mail Stop C-30
16811 El Camino Real
Houston, TX 77058

Dear Mr. Brose:

A software change request was issued by Mr. E. J. Jung and me on October 23, 1974, to incorporate changes into the thin skin heating rate data reduction computer program (THNSKN). Equation (2) of that document should be

$$q = \frac{1}{24} \frac{\rho C_p d}{t_{N-1}} \frac{N-1}{N-2} (T_{ij}^N - T_{ij}^{N-1} - T_{ij}^I - T_{ij}^2)$$

The expressions in equations (5) and (6) should be carrying a negative sign.

Please incorporate these corrections into the program.

C. D. Scott

LOCKHEED ELECTRONICS COMPANY, INC
AEROSPACE SYSTEMS DIVISION

16811 EL CAMINO REAL

HOUSTON, TEXAS 77058

TELEPHONE (AREA CODE 713) 488-0280

In reply refer to:
#121-8315-199
J.O. #83-157

December 31, 1974

TO: FD5/Chief, Data Processing Branch
FROM: LEC/Manager, Data Processing Systems Department
SUBJECT: Transmittal of EXEC VIII Version of the THNSKN Program

Transmitted herewith is the EXEC VIII version of THNSKN program for the Structures and Mechanics System. This version replaces the EXEC II version.

Results from the validation runs, after being checked for correctness with the use of LEC generated test data, were submitted to the customer, Dr. Carl Scott. Upon his acceptance, the Software Change Request was signed by the SIC and NASA Project Leader. The Software Change Request form is attached giving the descriptive reason for program modification.

W. N. Fitzpatrick
W. N. Fitzpatrick

NNF:JEM:jlb
Attachments

cc: H. Stephenson/FD53
D. L. McCormick/FD52
C. Scott/ES3
E. J. Jung/ES3
C. E. Hutchinson/C30
C. F. Iven/C11
[REDACTED]
J. Brose/C30
J. E. McFarland/C30
J. O. File

LOCKHEED ELECTRONICS COMPANY, INC
AEROSPACE SYSTEMS DIVISION

18811 EL CAMINO REAL

• HOUSTON, TEXAS 77058

• TELEPHONE (AREA CODE 713) 488 0380

In reply refer to:
#121-8315-199
J.O. #83-157

December 31, 1974

TO: FD5/Chief, Data Processing Branch
FROM: LEC/Manager, Data Processing Systems Department
SUBJECT: Transmittal of EXEC VIII Version of the THNSKN Program

Transmitted herewith is the EXEC VIII version of THNSKN program for the Structures and Mechanics System. This version replaces the EXEC II version.

Results from the validation runs, after being checked for correctness with the use of LEC generated test data, were submitted to the customer, Dr. Carl Scott. Upon his acceptance, the Software Change Request was signed by the SIC and NASA Project Leader. The Software Change Request form is attached giving the descriptive reason for program modification.

W. N. Fitzpatrick
W. N. Fitzpatrick

WNF:JEM:jlb
Attachments

cc: H. Stephenson/FD53
D. L. McCormick/FD52
C. Scott/ES3
E. J. Jung/ES3
C. E. Hutchinson/C30
C. F. Iven/C11
[REDACTED]
J. Brose/C30
J. E. McFarland/C30
J. O. File

SOFTWARE CHANGE REQUEST

Date Oct. 23, 1974

Requester/
Organization E.J.Jung/C.Scott/JSC-ES

Need Date Dec. 31, 1974

To Be Completed By Responsible Organization
Job Order <u>83-15</u> SCR No. <u>83-15-30</u>
Program Name <u>THNSKN</u>
Program No. <u>Q614</u>
Project No. <u>4300</u>
Target Date <u>12/31/74</u>

REASON FOR CHANGE:

To improve the accuracy and automation of the computer program THNSKN used to calculate heat fluxes from temperature time histories measured on thin skin heat transfer models tested in JSC arc tunnel facilities.

CHANGE DESCRIPTION (attach extra sheet if necessary):

See the attached description.

TO BE COMPLETED BY RESPONSIBLE ORGANIZATION

ESTIMATED RESOURCES:	APPROVALS BY:
Man-Hours <u>120</u>	<u>C.E. Jung</u> <u>11/11/74</u> Task Manager
Computer Hours <u>2.0</u>	<u>W.H. Scott</u> <u>11-12-74</u> Technical Monitor <u>P.L. Bellan</u> <u>11/14/74</u> Branch Chief

TRANSMITTAL TO PRODUCTION:

Submitted by:

Programmer	Date	Operating system
Validation approved by:		New program decks have been submitted to production
<u>C.E. Jung</u> <u>11-30-74</u>		Transmittal tape replaces current system CUR/PUR
System integration Coordinator	Date	Overlay production CUR/PUR with transmittal CUR/F
		Symbolic elements are contained in file number
		Relocatable elements are contained in file number
		No changes are required in execution deck setup
		Changes in run instructions are attached
NASA, Project Leader	Date	Transmitted program tape number

ACCEPTANCE BY PRODUCTION:

Date test
run completed

8-24

Project Leader Date

SOFTWARE CHANGE REQUEST

Date Oct. 23, 1974

Requester/
Organization E.J.Jung/C.Scott/JSC-ES

Need Date Dec. 31, 1974

To Be Completed By Responsible Organization
Job Order <u>83-15</u> SCR No. <u>83-15-50</u>
Program Name <u>THNSKN</u>
Program No. <u>Q614</u>
Project No. <u>4300</u>
Target Date <u>12/31/74</u>

REASON FOR CHANGE:

To improve the accuracy and automation of the computer program THNSKN used to calculate heat fluxes from temperature time histories measured on thin skin heat transfer models tested in JSC arc tunnel facilities.

CHANGE DESCRIPTION (attach extra sheet if necessary):

See the attached description.

TO BE COMPLETED BY RESPONSIBLE ORGANIZATION

ESTIMATED RESOURCES:

Man-Hours 120

Computer Hours 2.0

APPROVALS BY:

<u>C.E. Jung</u>	<u>11/11/74</u>
Task Manager	Date
<u>W. A. Scott</u>	<u>11-12-74</u>
Technical Monitor	Date
<u>J. E. Miller</u>	<u>11/14/74</u>
Branch Chief	Date

TRANSMITTAL TO PRODUCTION:

Submitted by:

Programmer	Date
Validation approved by:	<u>10/20/74</u>
System Integration Coordinator	<u>10/20/74</u>
MSA, Project Leader	Date

- Operating system
- New program decks have been submitted to production
- Transmittal tape replaces current system CUR/PUR
- Overlay production CUR/PUR with transmittal CUR/F
- Symbolic elements are contained in file number
- Relocatable elements are contained in file number
- No changes are required in execution deck setup
- Changes in run instructions are attached
- Transmitted program tape number

ACCEPTANCE BY PRODUCTION:

Date test
run completed

8-24

Project Leader Date

THIN SKIN PROGRAM MODIFICATION

Code modifications are required to improve the accuracy and automation of the computer program THNSKN used to calculate heat fluxes from temperature time histories measured on thin skin heat transfer models tested in the JSC arc tunnel facilities. The modification described here will also allow one discontinuity in the skin thickness (in one direction only) and uses finite difference expressions which are approximately second order accurate (except at end points) in both the space and time derivatives of the heat conduction equation.

The following modifications are required:

- 1) At present the computer program calculates heat fluxes only during one time period. Modify the program so that the number of time periods that heat fluxes are calculated during a run ~~from~~ may be specified in the input.
- 2) Compute the average heat fluxes for each time period and print the average for each location.
- 3) Remove the restriction that if bad thermocouples are at end points of rows or columns of thermocouples, the computation is ~~aborted~~. Use the next good thermocouple ^{as} at the end point.
- 4) Compute the conduction correction at end points (last good thermocouple) using the same conduction correction as at points adjacent to the end point. e.g., $\bar{q}_{bi1}^y = \bar{q}_{bi2}^y$
- 5) Allowance for discontinuity in skin thickness— In the input two skin thicknesses, d_1 and d_2 , are to be specified along with

the position y_d of the junction between the two thicknesses

$d = d_1$ for $y < y_d$ and $d = d_2$ for $y > y_d$

Use the appropriate thickness d for each location.

- 6) Compute the mean heat flux for each time interval using the formula

$$\bar{q}_{ij} = \bar{q}_{ij}^y + \bar{q}_{ij}^x + \bar{q}_{ij}^z \quad (1)$$

where:

$$\bar{q}_{ij}^y = \frac{16 \rho C_p d}{L_{ij} - L_i} \frac{N}{N-2} (T_{ij}^N + T_{ij}^{N-1} - T_{ij}^1 - T_{ij}^2) \quad (2)$$

$$\bar{q}_{ij}^x = \frac{24 K d}{x_{i+1,j} - x_{i-1,j}} \left(\frac{\bar{T}_{ij} - \bar{T}_{i-1,j}}{x_i - x_{i-1}} - \frac{\bar{T}_{i+1,j} - \bar{T}_{ij}}{x_{i+1} - x_i} \right) \quad (3)$$

$$\bar{q}_{ij}^z = \frac{24 K d}{y_{i,j+1} - y_{i,j-1}} \left(\frac{\bar{T}_{ij} - \bar{T}_{ij-1}}{y_j - y_{j-1}} - \frac{\bar{T}_{i,j+1} - \bar{T}_{ij}}{y_{j+1} - y_j} \right) \quad (4)$$

To compute \bar{q}_{ik}^y at thermocouple locations adjacent to the skin thickness jump (y_d) use the following formulas for $y_k < y_d < y_{k+1}$ instead of (4).

$$\bar{q}_{ik}^y = \frac{24 K d_1}{y_{k+1} - y_{k-1}} \left(\frac{\bar{T}_{ik-1} - \bar{T}_k}{y_k - y_{k-1}} + \frac{d_2 (\bar{T}_{ik+1} - \bar{T}_k)}{(y_d - y_k) d_2 + (y_{k+1} - y_d) d_1} \right) \quad (5)$$

$$\bar{q}_{i,k+1}^y = \frac{24 K d_2}{y_{k+2} - y_k} \left(\frac{d_1 (\bar{T}_k - \bar{T}_{ik+1})}{(y_i - y_k) d_2 + (y_{k+1} - y_d) d_1} + \frac{\bar{T}_{k+2} - \bar{T}_{i,k+1}}{y_{k+2} - y_{k+1}} \right) \quad (6)$$

The bars over the T's denote time average of the temperatures throughout a given interval. The superscripts on the T's in the first term denote the first, second, last, and next to last temperatures in the time interval. The number of samples in a time interval is N. The first time in the interval is t_1 , and the last is t_N . The latter two terms in equations (3) and (4) are the lateral heat loss terms as used previously except now they are averages over the time interval. This procedure will replace the one currently used in the code.

- 7) Output - Print the start and stop times for each time interval. Print out the number of times N in each interval, the times t_i and temperatures \bar{T}_{ij}^n at each time. No longer print the heat flux terms at each time since these are no longer calculated.

Print each of the terms in equation (1): \bar{q}_{ij} , \bar{q}_{ij}^x , \bar{q}_{ij}^y

and the net heat flux \bar{q}_{ij} . Continue to compute and print the linear least squares heat flux in the revised program. Finally, print the mean of \bar{q}_{ij} averaged over the number of time intervals specified in the input.

- 8) Amend program documentation to reflect these and any previous changes.

ATTACHMENT 9

DIAGNOSTIC MESSAGES

DIAGNOSTIC MESSAGES

FEWER POINTS THAN REQUESTED

This message occurs at the end of a time slice when the number of points accumulated for least squares heat flux computations is less than the requested (NTME). This is not necessarily abnormal.

PARITY ERROR RECORD DELETED

An input record has been skipped because of parity errors.

END OF FILE ENCOUNTERED ON UNIT 8. PROCESSING OF ACCUMULATED DATA WILL BE ATTEMPTED.

Normally, stop times or stop event levels should be chosen so that the end-of-file is never encountered. If at least three scans of data have been accumulated, processing will be done.

TOO FEW POINTS AVAILABLE FOR CURVE FIT

Fewer than three data points have been stored so no least squares heat flux computations can be done.

***ERROR - NX OR NY IS BAD

Either one or both of NX and NY are too large or too small. Currently, the maximum size for either is 50. Either NX or NY must have a minimum value of 3.

Examples: NX NY

1	3	Valid
3	1	Valid
2	2	Invalid
1	50	Valid
51	51	Invalid

***ERROR - NTME IS LARGER THAN NN

The requested number of points to be used for least squares heat flow computations exceeds array dimensions (NN). Currently NN is 50.

***ERROR - TOO MANY CHANNELS

The number of channels specified for the input tape is too large for the array dimensions. Currently, the maximum number of channels which can be processed is 260.